



# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

A THREE-DIMENSIONAL TRANSONIC, POTENTIAL FLOW  
COMPUTER PROGRAM, ITS CONVERSION TO IBM  
FORTRAN AND UTILIZATION

by

Jack Paschall III

December 1983

Thesis Advisor:

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extensive; therefore, an interactive program was developed to aid the user in building the required input data file.

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A Three-Dimensional Transonic, Potential Flow Computer  
Program, Its Conversion to IBM Fortran and Utilization

by

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Submitted in partial fulfillment of the  
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## A B S T R A C T

This thesis describes the conversion of a computer program from Fortran IV for the NOS 1.2 operating system of the CYBER 175 or CDC 6600 computer to Fortran IV compatible with the Naval Postgraduate School IBM 3033 system. The converted program, called FLO27, calculates the inviscid, three-dimensional transonic potential flow over wings or wing-body combinations. The data input to FLO27 is extensive; therefore, an interactive program was developed to aid the user in building the required input data file.

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## I. INTRODUCTION

In the Aeronautical Engineering curriculum graduate level aerodynamics course, AE-4501, the students are exposed to two computer programs. One of these, prepared by the Douglas Aircraft Company, analyzes the potential flow around three-dimensional wings but is limited to incompressible flow [Ref. 1]. The other program, prepared by Cebeci, calculates the friction drag for two dimensional incompressible flow over airfoils [Ref. 2]. A serious defect of these programs is that they are not state-of-the-art computer programs. The Douglas program does not consider the effects of compressibility and the boundary layer program, in addition to being restricted to incompressible flow, does not predict the laminar to turbulent transition point.

### A. BACKGROUND

In 1980 the Department of Aeronautics at the Naval Postgraduate School acquired an intricate computer program recently developed by the Boeing Commercial Airplane Company. This state-of-the-art program calculates three-dimensional transonic flow over wings and bodies in

both the outer-inviscid flow region governed by the transonic potential equation and the thin layer in which the first order, compressible boundary layer equations are assumed to be valid.

The Boeing program as received was designed to be executed on a CDC 6600 or a CYBER 175 computer and was written using CDC FORTRAN IV extended language. This thesis therefore was primarily concerned with the conversion of the program to FORTRAN IV extended compatible with the Naval Postgraduate School's (NPS) IBM 3033 system. The large modular program was divided so that the potential flow analysis portion could be run separately. Simplified instructions for use of the program were also prepared.

#### B. VISCOUS/INVISCID SYSTEM OF PROGRAMS

The Viscous/Inviscid Wing System (VIWS) of programs calculates three-dimensional transonic flow over wings and wing body combinations including details of the laminar or turbulent flow in the three-dimensional viscous boundary layer. The flow field is calculated in two overlapping regions: an outer inviscid flow region governed by the transonic potential equation, and a thin boundary layer in which the first order, three-dimensional, compressible

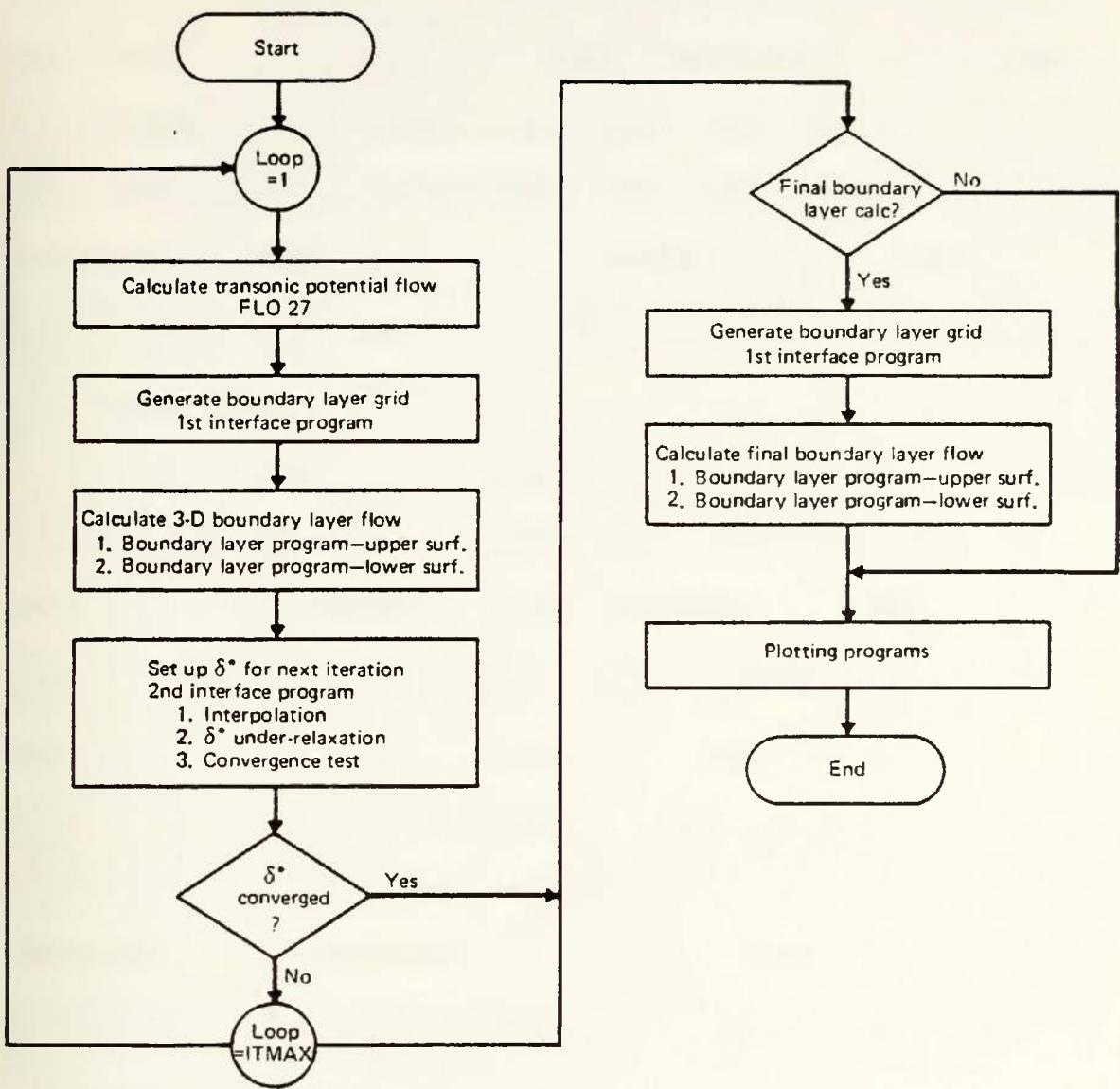
boundary layer equations are assumed to hold and in which the effects of surface heat and mass transfer can be computed. A list of the VIWS of programs is presented in Table I.

TABLE I

Viscous/Inviscid Wing System of Programs

Program Name	Description
FIC27	Jameson-Caughey inviscid, transonic wing code
A411IN	Reads geometry & velocity data, constructs coordinate system
VWIN	Potential flow boundary layer interface
A411AC1	Three-dimensional boundary layer program
INTERP	Boundary layer potential flow interface
A411P1 A411D2 A411FS	Graphics display programs

The basic sequence of calculations used by the VIWS to obtain matched viscous and inviscid solutions consists of an iterative loop in which the inviscid outer flow analysis and the boundary layer analysis are performed sequentially. The iterative sequence is continued until either convergence (satisfactory matching) is achieved, or the maximum number of iterations specified by the user has been performed. The VIWS programming sequence is shown schematically in Fig. 1.1.



**Figure 1.1. Viscous/Inviscid Interaction Procedure**

The potential flow is calculated for the bare wing during the first iteration. In subsequent iterations, the effect of the boundary layer flow on the outer inviscid flow is

felt as a modification to the wing shape through the addition of the boundary layer displacement thickness. Convergence is recognized, and the iterations are stopped, when the maximum change between the new and old displacement thickness, expressed as a fraction of the maximum displacement thickness, is less than the convergence tolerance chosen by the user.

The VIWS utilizes the Jameson-Caughey transonic inviscid wing program FLO27, to carry out the potential flow analysis. The boundary layer analysis is performed by a finite difference boundary layer prediction program developed by the Boeing Commercial Airplane Company. The basic theory behind the boundary layer program is contained in [Ref. 3]. A detailed description of the VIWS of programs (excluding the potential flow program FLO27) is contained in [Ref. 4]. A basic guide to the use of the VIWS of programs is contained in [Ref. 5].

### III. POTENTIAL FLOW PROGRAM FLO27

Because of the extensive length and number of program modules in the VIWS, the Potential Flow Program, FLO27, was singled out for conversion. It was anticipated that FLO27 would be run separately at first and recombined with the other program modules at some later date when these modules were themselves translated for execution on the IBM 3033 computer.

#### A. RE-PROGRAMMING

The Potential Flow Program, hereafter called FLO27, was received on magnetic tape and loaded into the IBM 3033 mass storage system using the Job Control Language (JCL) routines presented in Appendix A. The magnetic tape contained twenty (20) total files in which the format was 9 track, 1600 CPI, unlabeled. The card image format for the sixteen (16) program files is 80 characters per record and the four (4) output files contain 150 characters per record. The program and output files on the original CDC tape are listed in Table II.

The FLO27 program was converted to FORTRAN IV extended suitable for execution on the IBM computer using the NPS CDC

TABLE II  
CDC Magnetic Tape Files

File/Records	Name	Description
1 / 2356	FLO27	Potential Flow Program
2 / 3194	A411IN	Reads geometry & velocity data constructs coordinate system
3 / 378	VWIN	Potential flow boundary-layer interface
4 / 6611	A411AO1	Three-dimensional boundary layer program
5 / 1977	INTERP	Boundary-layer potential flow interface
6 / 688	A411PS	Streamline plots
7 / 211	A411P1	One-dimensional plots
8 / 586	A411P2	Contour plots
9 / 70	COUPLE	Procedure files
10 / 158	ITER	
11 / 7	DATAIN	
12 / 78	FINAL	
13 / 434	BOEB1	Boeing McLean computer program
14 / 36	CONIPLT	Contour plots
15 / 17	CORDPLT	One-dimensional plots
16 / 40	STREPLT	Streamwise plots
17	OUTF27	Output from FLO27
18	OUTIFC	Output from VWIN
19	OUT411L	Output from boundary-layer, lower surface
20	OUT411U	Output from boundary-layer, upper surface

to IBM conversion guide [Ref. 6]. The first step taken consisted of program compilation using the WATFIV compiler with its extended error messages. The listing which was

produced flagged all areas of the program which required revision. Program changes were accomplished utilizing this WATFIV listing. Some of the more general and repetitive changes are listed in Table III.

TABLE III  
FLO27 Re-Programming Changes

CDC Code	IBM Code Change
Variables: FREAD, FREAF, FWRIT, FWRIIF, IREAD, IREAF, IWRIT, IWRIF	Eliminated from program
WRITE(IWRIT,600)	WRITE(6,600)
READ(IREAF,500)	READ(5,500)
READ 7, WRITE 7 or REWIND 7	Changed to READ 14, WRITE 14 or REWIND 14
Call SECCND(T)	Step eliminated
Call SSWITCH(1,ISTOP)	Call SLITET(1,ISTOP)
Delimiter of form *	Replaced by '
Comment cards with *	Replaced by C
LEVEL statement	Step eliminated
If(UNIT(N).GT.0.) GO TC	All of this type eliminated

The most difficult change to make occurred with the CDC Buffer IN or Buffer OUT statements which were used in the program to transfer portions of a three-dimensional array into and out of main memory. The Buffer routines reduce the memory size required to execute the program. This statement type occurred in the main program and several of the subroutines.

The change required to translate this statement is presented below with the CDC code preceding the IBM FORTRAN.

BUFFER OUT (N3,1) (G(1,1,1),G(MX,MY,1)) changed to  
WRITE(N3) ((G(I,J,1),I=1,MX),J=1,MY) and  
BUFFER IN (N1,1) (G(1,1,M),G(MX,MY,M)) changed to  
READ(N1,ERR= ) ((G(I,J,M),I=1,MX),J=1,MY)

The variable ERR was assigned the GO TO statement number of the UNIT statement immediately following the BUFFER IN line of code. As an example, if the UNIT statement following the BUFFER IN code was - IF(UNIT(N1).GT.0.) GO TO 151, then the number 151 was assigned to variable ERR following the equal sign. All CDC UNIT statements were eliminated from the FLO27 source code per Table II.

In addition to the program changes required to run FLO27 on the IBM computer, several lines of code were added to modify the output format to a more usable form. A subroutine, VERTEC, which calls the Versatec plotter was also added to enhance program usefulness. This plotting routine is user controlled through an input variable and is explained in the next section. The modified FLO27 program source code is presented in Appendix E.

To facilitate program data entry several input variables which had recommended values were initialized to these values within the Main program and the subroutine GEOM. The initialized input variables and their values are presented in Table IV.

TABLE IV  
Initialized Input Variables

AREA	VARIABLE NAME	INITIALIZED VALUE
MAIN Prgm.	XSCAL	0.0
	PSCAL	0.0
	FCONT	0.0
	P20	0.7
	P30	1.0
	FSMCO	0.0
	PTMAP	0.0
	BLCP	0.0
	WEIG	1.0
	PTCK	0.0
Subrt. GEOM	FIX	0.0
	YSYM	0.0
	FNB	2.0
	PX	0.0
	PZ	0.0
	TRL	0.0
	SLT	0.0
	XSING	0.0
	YSING	0.0

A complete description of each input variable in Table IV can be found on pages 19 through 23 of [Ref. 5].

#### B. PROGRAM DESCRIPTION

The FLC27 program is a computer code written to analyze the transonic flow over a wing alone or a wing on a cylindrical fuselage. It uses a finite-volume formulation to solve the exact potential flow equation in conservative form. In the development of the equations, the basic assumptions are; steady flow, no heat or work transfer, isentropic flow, irrotational flow, no body forces and a perfect gas. The velocity vector in cartesian coordinates is

$$\vec{V} = u\hat{i} + v\hat{j} + w\hat{k} \quad (2.1)$$

where  $u$ ,  $v$  and  $w$  are the velocity components. The continuity equation, assuming steady flow, is

$$\frac{\partial}{\partial x}(\rho u) + \frac{\partial}{\partial y}(\rho v) + \frac{\partial}{\partial z}(\rho w) = 0 \quad (2.2)$$

Next a velocity potential is introduced such that the velocity components are calculated as the gradient of this potential.

$$u = \phi_x, \quad v = \phi_y, \quad w = \phi_z \quad (2.3)$$

With the introduction of the velocity potential, the continuity equation 2.2 becomes

$$\frac{\partial}{\partial x}(\rho \phi_x) + \frac{\partial}{\partial y}(\rho \phi_y) + \frac{\partial}{\partial z}(\rho \phi_z) = 0 \quad (2.4)$$

Assuming no heat or work transfer, the energy equation can be written as

$$T \left[ 1 + \frac{(\gamma - 1)}{2} M^2 \right] = T_{\infty} \left[ 1 + \frac{(\gamma - 1)}{2} M_{\infty}^2 \right] \quad (2.5)$$

The flow is assumed to be uniform in the far field. On the surface of the body, the normal velocity component is zero. The velocities and densities of the near field are normalized using the free stream velocity and density, thus  $v_{\infty} = 1$  and  $\rho_{\infty} = 1$ . Using the assumptions that the flow is isentropic and a perfect gas, the energy equation 2.5 can be shown to be

$$\rho = \left[ 1 + \frac{(\gamma - 1)}{2} M_{\infty}^2 \left( \frac{1}{1 - v^2} \right) \right]^{\frac{1}{\gamma - 1}} \quad (2.6)$$

With equations 2.5 and 2.6 there are only two unknowns,  $\phi$  and  $\rho$ . They can be solved, subject to the boundary condition of flow tangency, using a finite volume technique. The basic numerical scheme for the solution is the

construction of a mesh from small volume elements (cubes) which are packed around the wing or wing-body configuration. The cubes in the computational domain are separately mapped to distorted cubes in the physical domain by independent transformations from local coordinates X, Y and Z to Cartesian coordinates x, y and z. The mesh points are the vertices (corners) of the mapped cubes. The velocity potential and density are calculated at each vertex in the mesh. The pressure distribution can then be calculated from

$$P = \frac{\rho \sigma}{\gamma M_\infty^2} \quad (2.7)$$

In the event that the local flow velocity becomes supersonic and shocks occur, these are handled in the usual manner by insuring that:

- 1) The tangential velocity components are equal on each side of the shock.
- 2) Continuity is maintained by keeping the product of  $\rho U_n$  constant across the shock (where  $U_n$  is the normal velocity component).
- 3) Discontinuous expansions (corresponding to an "expansion shock") are excluded from the flow field.

The assumption of isentropic flow along with the existence of shocks presents a contradiction which can only be resolved by limiting the flow to very weak shocks for which entropy and vorticity generation may be ignored. Thus, solutions will be valid only for subsonic free stream velocities.

The main three-dimensional array containing the potential function data is stored on disk, and special unformatted input/output statements are used to bring planes of data into central computer memory and to store updated planes of data back on the disk. In the construction of the computational coordinate system, a Joukowski transformation is used to transform the cylindrical fuselage to a vertical slit and then a sheared parabolic transformation is used in planes containing the airfoil sections. A detailed mathematical formulation of the potential flow analysis is contained in [Ref. 7].

### 1. Program Input

The input to FLO27 consists of variables which are read with an 8F10.6 FORMAT. Each input card has a title card which precedes it. This title card contains the input variable name and effectively labels the input data for easy

reference. The title for each input data is placed in the same column as the input data it labels. The title cards are read with a 20A4 FORMAT. All numerical input values are real numbers. The following data deck, listed card by card, is the minimum input data required for a simple wing analysis. Each "card" can be interpreted as one line of data on your terminal. A complete sample data set is presented in Appendix C.

CARD 1 The Run Title (64 characters maximum)

CARD 2 Title card for the input variables

FNX, FNY, FNZ, FMESH and FPLOT

CARD 3

Cols. 1-10 FNX - Number of computational cells in the chordwise direction for the initial mesh.

MAX =  $160/2^{**n}$ , where n = FMESH - 1. (See Cols. 31-40 for FMESH)

Cols. 11-20 FNY - Number of computational cells in the normal direction from the airfoil surface for the initial mesh.

MAX =  $16/2^{**n}$ , where n = FMESH - 1.

Cols. 21-30 FNZ - Number of computational cells in the spanwise direction for the initial mesh.

MAX =  $32/2^{**n}$ , where n = FMESH - 1.

Cols. 31-40 FMESH - Determines the number of times a program generated computational mesh is refined. Enter only 1.0, 2.0 or 3.0 for coarse, medium or fine mesh. If 3.0 is selected the program will calculate flow over the wing for the coarse mesh then half the mesh size (medium), recalculate, then half the mesh again (fine) and do a final potential flow calculation. Output parameters are printed for each mesh size for which calculations were performed.

Cols. 41-50 FELOT - Output flag

0.0 = Normal output without printer-plot of Cp

1.0 = Normal output with printer-plot of Cp  
at each computational mesh point for  
each wing section.

2.0 = Normal output with Versatec plots of  
Cp versus X/C for each wing section of  
the final mesh.

CARD 4 Title card for the input variables

FIT, COVO and P10

CARD 5-M One card for each computational mesh. Total  
number of cards equal to M = FMESH.

Cols. 1-10 FIT - A parameter which fixes the maximum number of iterations the program will use to converge the velocity potential to a specified tolerance (COVO). This parameter must be repeated for each mesh refinement.

Cols. 11-20 COVO - Velocity potential convergence criteria. This input variable is also entered for each selected mesh. A value of 0.000001 is recommended.

Cols. 21-30 P10 - This parameter determines the subsonic point relaxation factor for the specified mesh size. A value of less than 2.0 must be entered for each designated mesh. Recommended values are: 1.6 for coarse, 1.3 for medium and 1.2 for the fine mesh.

CARD 6 Title card for the input variables

FMACH, YA, AL and CDO

CARD 7

Cols. 1-10 FMACH - Free stream Mach number

Cols. 11-20 YA - Yaw angle in degrees

Cols. 21-30 AL - Angle of attack in degrees

Cols. 31-40 CDO - Drag coefficient due to skin friction. Unless known, an estimated value of 0.01 is recommended.

CARD 8 Title card for the input variables

ZSYM, FNS, SWEEP, DIHED and FUS

CARD 9

Cols. 1-10 ZSYM - The wing planform symmetry trigger.

0.0 = Yawed wing, has no spanwise symmetry

1.0 = Swept wing, has spanwise symmetry

Cols. 11-20 FNS - This input variable tells the program the total number of wing sections you have selected to define the wing half span. The number must be at least three (3) but not more than eleven (11) sections.

Cols. 21-30 SWEEP - Leading edge sweep angle in degrees.

Cols. 31-40 DIHED - Dihedral angle in degrees. See Fig. 2.1.

Cols. 41-50 FUS - Input the fuselage radius. Enter 0.0 for a wing-alone case.

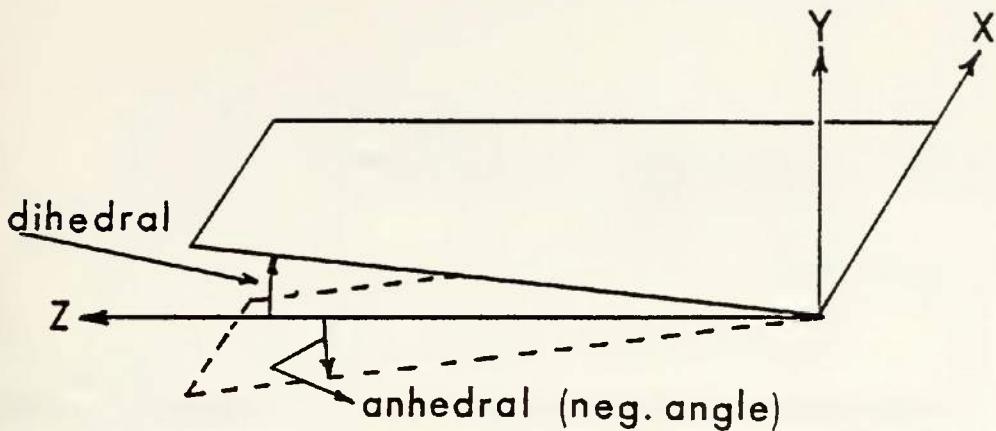


Figure 2.1. Dihedral Angle

Data input cards from 10 through 15 are used for defining wing planforms and section geometrics. For the first wing section, all data cards from card 10 through card 15 must be used. For the second and subsequent sections there is an option for skipping the wing section defining data (cards 12 through 15) and copying the data from that of the previous section. This option is controlled by the input variable FSEC. If this option is not used, data cards from 10 through 15 must be repeated for each wing defining section. The number of wing sections which are defined is input with the variable FNS. Remember, up to 11 sections may be defined, and a minimum of 3 sections must be defined. All wing planform and section defining geometrics must be in consistent units. Wing planform and section defining quantities are presented in Fig. 2.2.

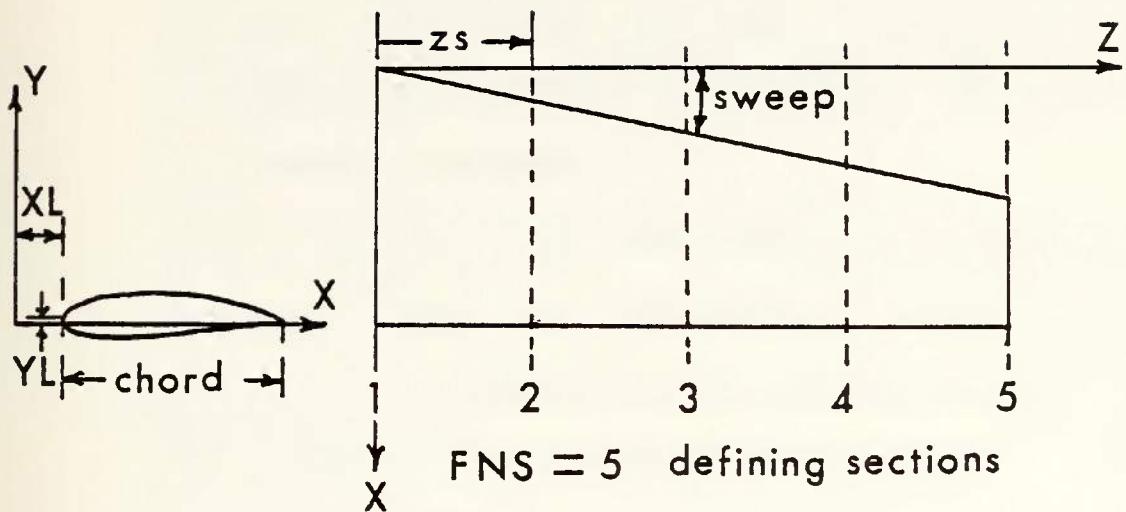


Figure 2.2. Wing Defining Geometry

CARD 10 Title card for the input variables

ZS, XI, YL, CHORD, THICK, AT and PSEC

CARD 11

Cols. 1-10 ZS - The section spanwise coordinate

(Start at the centerline and work  
outboard)

Cols. 11-20 XL - Section leading edge X coordinate

Cols. 21-30 YL - Section leading edge Y coordinate

Cols. 31-40 CHORD - Section chord length

Cols. 41-50 THICK - The thickness scaling factor can be used to scale all Y coordinates of the wing section. Thus percent thickness and camber are increased (or decreased) accordingly. Use 1.0 if no scaling is desired.

Cols. 51-60 AT - The twist angle of each section (geometric twist) measured from the X axis to the chord line. A positive twist angle reduces the section angle of attack and gives "washout". Use 0.0 for no twist.

Cols. 61-70 FSEC - This is a flag which determines whether or not the program reads wing section defining geometry from a previous wing section or from new defining geometry. For the first section defined you must set FSEC to 1.0. Following the first section, if you define new section geometry then use FSEC = 1.0. If you want the program to read the section geometry defined from the previous section then set FSEC = 0.0.

CARD 12 Title card for the input variable

FN

CARD 13

Ccls. 1-10 FN - This variable contains the number of points which define the upper and lower surface of the section. A maximum of 161 points may be used.

CARD 14 Title card for the input variables

XP(I) and YP(I)

CARDS 15-1 to 15-N Total number of cards equals N,

where N = integer part of  $(FN+2)/3$ .

The X and Y coordinates at each point are entered in pairs, three points to a card. (See Appendix C for sample input)

Ccls. 1-10 XP(I) - X coordinate of the wing  
section point

11-20 YP(I) - Y coordinate of the wing  
section point

21-30 defining X coordinate for next  
point

31-40 defining Y coordinate for next  
point

41-50 defining X coordinate for  
following point

The X and Y coordinates of the wing section defining points must be entered starting with the upper surface trailing edge point and proceeding along the upper surface to the leading edge, and returning along the lower surface to the lower surface trailing edge point. It is very important to define the section leading edge with a large number of closely spaced points. Suggest at least 0.05 spacing or less between X coordinate values from 0.1 X/C to the leading edge,  $X/C = 0.0$ . Each X and Y coordinate point is normalized using the chord length for that section. Section defining geometrics are illustrated in Fig. 2.3.

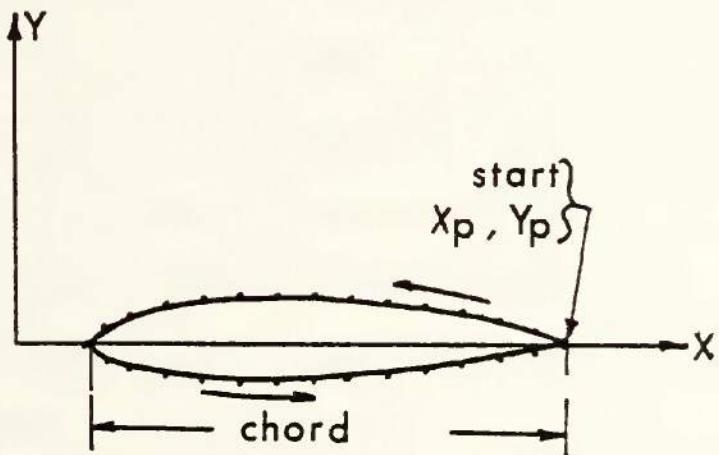


Figure 2.3. Section Defining Geometry

CARD 16 Title card containing the words in Cols. 1-80

END OF CALCULATIONS

CARD 17 Title card for the input variable

FNX

CARD 18

Cols. 1-10 FNX - This variable indicates the end of a set of calculations and must be set equal to 0.0. Its purpose is to indicate that the program has run to completion.

## 2. Program Output

Output from the FLC27 program varies with the value of the input variable FPLCT. When FPLOT is set equal to 0.0 a normal output is produced. This normal output contains (in order of occurrence): refined input geometry data including trailing edge slope and angle calculations; iterative solution of the potential flow mesh; section characteristics and wing characteristics. The iterative solution, section and wing characteristic data are repeated for each mesh refinement requested. Thus, if the input variable FMESH is set equal to 3, these data are calculated and output three times. The last data in the normal output consists of the non-dimensionalized chord (X/C) and pressure

coefficient ( $C_p$ ) data at each computational mesh point for each wing section calculated during the final mesh. A sample of the normal output data is presented in Appendix D and represents the output data from Appendix C input data.

If variable FPLOT is set equal to 1.0, the output data is increased considerably. This output contains the normal output plus a line printer-plot of the pressure coefficient at each computational mesh point for each wing section. The line printer-plot is produced for each wing section of each mesh refinement. The length of the output data with FPLOT set equal to 1.0 can approach 6000 records depending on the number of mesh refinements requested. These plots are of questionable value and, therefore, an alternate plotting program was developed.

When the variable FPLOT is set equal to 2.0, the normal output data is produced plus a Versatec plotting subroutine (VERTEC) is called. The subroutine outputs, via the Versatec plotter, plots of  $C_p$  versus  $X/C$  for each wing section of the final mesh calculations. This routine is simply putting into plot form the  $C_p$  and  $X/C$  numerical data contained in the normal output. A sample of the Versatec plot is presented in Fig. 2.4.

## SECTION CP DATA

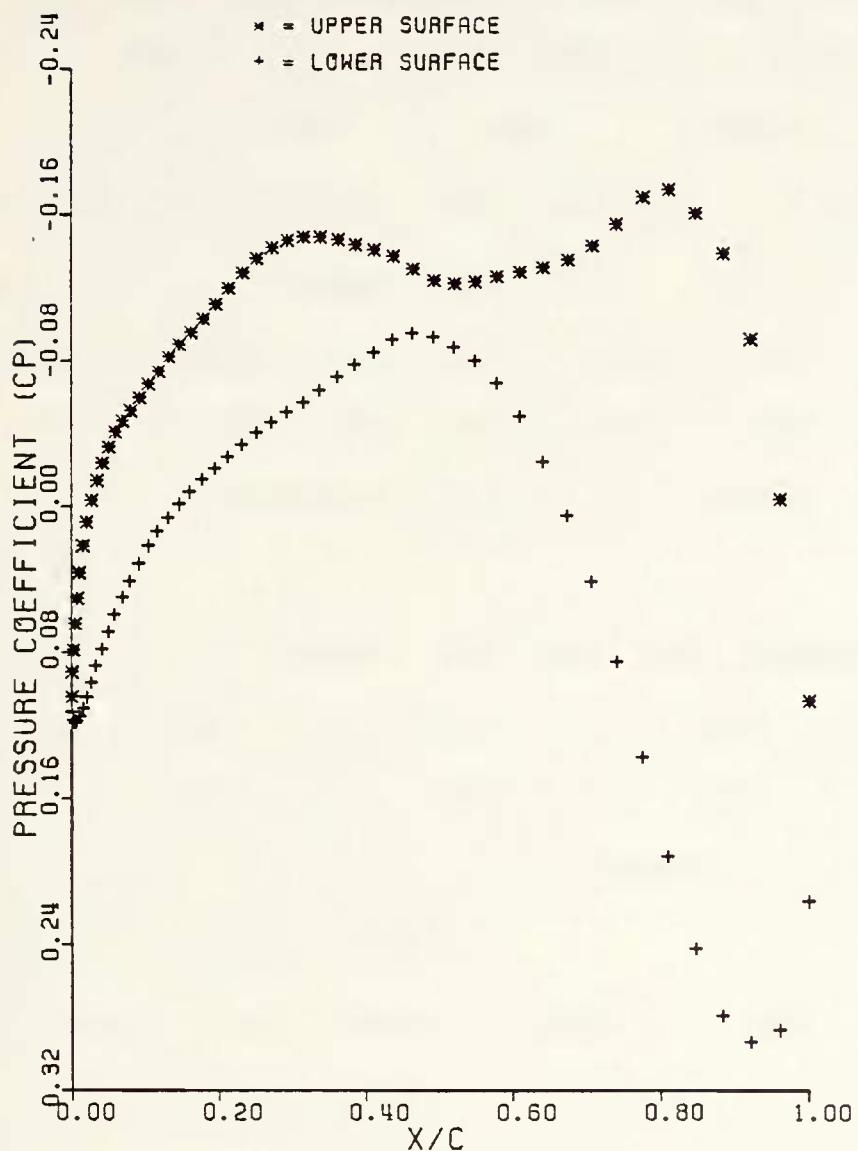


Figure 2.4. Versatec Plot of Cp vs. X/C

### III. INTERACTIVE INPUT PROGRAM FLO27IN

The input data file required for the FLO27 program is extensive. Errors in input data FORMAT will cause program errors at execution time. In order to eliminate these errors and reduce the input data workload, a computer terminal interactive program was written. This interactive program, called FLO27IN, is a user-friendly way of creating an input data file for the potential flow wing analysis program FLO27. The FLO27IN program source code is presented in Appendix F.

The interactive program, FLO27IN, when executed ask's questions of the user in order to construct and write to the user's "A" disk the required FLO27 input data file. The following presents the step-by-step procedure for executing the interactive program FLO27IN.

STEP #1---Log on to any IBM 3033 interactive terminal  
with your user number and password.

STEP #2---Once logged on and in the CMS operation mode  
type:

**CP LINK 0247P 191 120 RR** then hit ENTER

STEP #3---The word PASSWORD will appear, Type and ENTER  
**AERO**

STEP #4---Type and ENTER

ACC 120 D

STEP #5---Type and ENTER

LOAD FLO27IN (START)

The screen will display the header for the interactive program. Answer each question presented. At the end of each question in parenthesis is the input data variable associated with that question and whether the input parameter is a real number (R) or an integer (I). Example:  
==> Enter the free stream Mach number (FMACH): (R). FMACH is the input data variable for the question. As you proceed through the FLC27IN program, opportunities to review and change input data will be presented. Should it become necessary to change your input data after completing the FLO27IN program, you can simply XEDIT the created data file.

The FLO27IN program also incorporates a library which contains the wing-section defining data for a number of current wing shapes. A copy of this library is presented in Appendix B. This feature will be displayed during program execution by the use of a menu from which the user can select a pre-defined wing section or define his own.

Upon completion of user inputs to the interactive program three additional data lines are automatically written to the bottom of the input file. They are:

END OF CALCULATION

FNX

0.0

In addition, Job Control Language (JCL) cards are written to the top and bottom of the file. All JCL cards start with a // format. After FLO27IN has run to completion type and enter RELEASE 191 to release the aero disk which was linked while executing the FLO27IN program. The created data file is written to the user's "A" disk with <filename> <filetype> of FLO27 DATAIN. Additional changes can be made simply by entering the XEDIT mode and editing the file.

#### IV. FLO27 BATCH SYSTEM EXECUTION

The potential flow program FLO27 can be executed after the input data file has been created. The batch processor is required for FLO27 execution because of the extensive CPU time needed to run the program. While in the XEDIT mode, a standard JCB card must be added to the top of the FLO27 DATAIN file prior to submission for job execution. The JOB card has the form:

//jobname JOB (nnnn,pppp),'ident',CLASS=J

jobname = may contain up to 8 alphanumeric characters,

the first of which must be alphabetic.

nnnn = your user number

pppp = project number, assigned by professor

'ident' = contains the user's own identification

information. A maximum of 20 characters may be contained within the single quotation marks.

After adding the JOB card to your data file, you are ready to execute the program. Type SUBMIT FLO27 DATAIN and press ENTER. Batch runs are normally not worth waiting for. To inquire about the status of the job, enter INQ and the job name used on the JOB card or "logoff". If the system is busy and the maximum mesh size was selected, it may be several hours before your job is run.

When the job is run the output will be spooled to the batch printer located next to the VM printer in the main computer building. The title at the top of the printout for batch jobs is the name entered on the JOB card. If it is desired to have the program output data spooled directly to the terminal, it will be necessary to add one additional JCL card to the input data set. This card must be placed immediately following the JOB card and has the form:

```
//*MAIN ORG=NPGVM1.nnnnP
```

where nnnn = your user number

Inserting this card in the input data will cause all program output to be spooled to the user's virtual reader where it may be looked at, printed or transferred to his "A" disk. To enquire as to whether information is in the reader simply type RDR and hit enter, then follow the instructions on the screen.

## V. PROGRAM TEST RESULTS

The FLC27 program was tested in three stages; (1) during the reprogramming phase for conversion completeness, (2) after successful conversion with suitable wing data for program accuracy and (3) during an AE-4501 class project.

### A. ACCEPTANCE TEST DATA

To test and ensure that the FLO27 program was converted to IBM compatible Fortran without error, an acceptance test data set was used. The acceptance test input and output data was supplied with the original CDC program source code. After conversion of the FLO27 program to Fortran suitable for the NPS IBM system, the acceptance test input data were run and the output results compared to the output generated by the CDC system.

Both output data sets were numerically exact when the FLO27 program was run in double precision on the IBM system. If the program was run in single precision, the numerical output values were exact to the third decimal place. The difference in single precision accuracy occurs because the CDC system uses a 64 bit word length while the IBM system word length in single precision is only 32 bits. It was

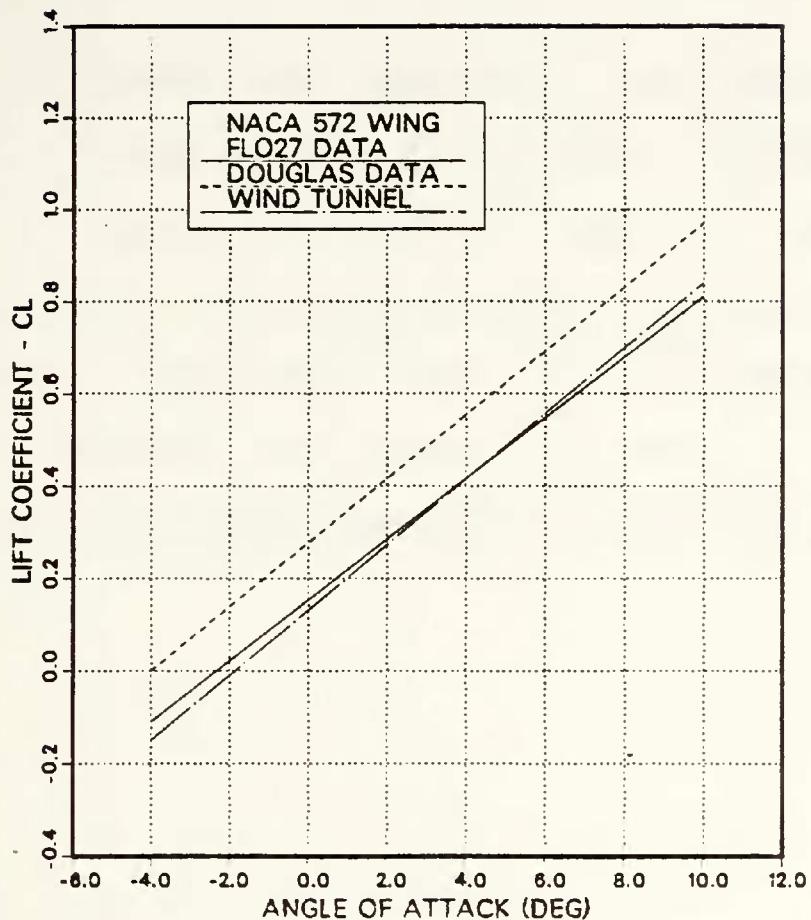
decided that the IBM single precision accuracy was satisfactory.

#### B. COMPARISON WITH OTHER PROGRAMS

The FLC27 program was also tested for accuracy by using the wing planform and section data from a NACA 572 wing. The data were run on both the FLO27 program and the Douglas potential flow program [Ref. 1]. The data generated by both programs was compared to wind tunnel data for the NACA 572 wing [Ref. 8]. The results are presented in Fig. 5.1 as plots of lift coefficient versus angle-of-attack. The results show that for the NACA 572 wing the FLO27 program more accurately predicts the wing lift coefficient than does the Douglas program.

#### C. AE-4501 CLASS PROJECT

The final test phase was conducted by introducing the FLO27 program into the AE-4501 course as a class project. This was accomplished to determine student problems/comments concerning the data input program FLO27IN and to test an additional wing shape. The wing chosen for study was that of the A-7 airplane. The A-7 wing has a distinct leading edge notch at the approximate mid-span. When the planform geometry was run with the notch included the FLO27 program



**Figure 5.1. Program Calculated and Wind Tunnel Data**

ran to completion but gave negative values for section and total induced drag coefficient. The value for the lift coefficient was low for the freestream Mach and angle-of-attack used. It was found that if the notch was

excluded from the wing geometry input data the program results were satisfactory both for induced drag and lift coefficient.

From the AE-4501 class experience it was determined that sharp wing planform discontinuities cannot be handled by the program. If however, the changes in shape are gradual, such as a wing glove, the program output appears to be satisfactory. Such was the case with the acceptance test case data where the wing geometry was that of the F-8 supercritical wing which incorporates a wing glove.

## APPENDIX A

C This JCL routine allocates sufficient space on the mass  
C storage system to store the entire tape contents  
//JACK JOB (3266,0178), 'PASCHALL-2759', CLASS=A  
// \*MAIN ORG=NEGVM1. 3266 P  
// EXEC PGM=IEFBR14  
// DD1 DD UNIT=3330V, MSVGP=PUB4C, DISP=(NEW,CATLG),  
// DSN=MSS.S3266.WFLOW.DATA,SPACE=(CYL,(16,4,2))  
/\*  
//

C This JCL routine is used to transfer all tape files to  
C a partitioned data set in the mass storage system  
//JACK JOB (3266,0178), 'PASCHALL-2759', CLASS=J  
// \*MAIN ORG=NEGVM1. 3266 P  
// COPY PROC FILE=, MEM=  
// EXEC PGM=IEBGENER  
// SPRINT DD SYSOUT=A  
// SYSIN DD DUMMY  
// SYSUT1 DD UNIT=3400-6, VOL=SER=WFLOW, DISP=(OLD,PASS),  
// LABEL=(&FILE,BLP,IN)  
// DCB=(RECFM=F,BLKSIZE=80, DEN=3, OPTCD=Q)  
// SYSUT2 DD DISP=(OLD,KEEFL,  
// DSN=MSS.S3266.WFLOW.SOURCE(&MEM),  
// DCB=(RECFM=FB, LRECL=80, BLKSIZE=6400)  
// PEND  
// EXEC COFY,FILE=1, MEM=FLO27  
// EXEC COFY,FILE=2, MEM=A411IN  
// EXEC COFY,FILE=3, MEM=VWIN  
// EXEC COFY,FILE=4, MEM=A411AO1  
// EXEC COFY,FILE=5, MEM=INTERF  
// EXEC COFY,FILE=6, MEM=A411PS  
// EXEC COFY,FILE=7, MEM=A411P1  
// EXEC COFY,FILE=8, MEM=A411P2  
// EXEC COFY,FILE=9, MEM=COUPLE  
// EXEC COFY,FILE=10, MEM=ITER  
// EXEC COFY,FILE=11, MEM=DATAIN  
// EXEC COFY,FILE=12, MEM=FINAL  
// EXEC COFY,FILE=13, MEM=BOEB1  
// EXEC COFY,FILE=14, MEM=CONTPLT  
// EXEC COFY,FILE=15, MEM=CORDPLT  
// EXEC COFY,FILE=16, MEM=STREPLT  
// COPY2 PROC FILE=, MEM=, LRECL=80, BLK=6400  
// EXEC PGM=IEBGENER  
// SPRINT DD SYSOUT=A  
// SYSIN DD DUMMY  
// SYSUT1 DD UNIT=3400-6, VOL=SER=WFLOW, DISP=(OLD,PASS),  
// LABEL=(&FILE,BLP,IN)  
// DCB=(RECFM=F,BLKSIZE=&LRECL, DEN=3, OPTCD=Q)  
// SYSUT2 DD DISP=(OLD,KEEFL, DSN=MSS.S3266.WFLOW.DATA(&MEM),  
// DCB=(RECFM=FB, LRECL=&LRECL, BLKSIZE=&BLK)  
// PEND  
// EXEC COFY2,FILE=17, LRECL=150, BLK=6000, MEM=OUTF27  
// EXEC COFY2,FILE=18, LRECL=150, BLK=6000, MEM=OUTIFC  
// EXEC COFY2,FILE=19, LRECL=150, BLK=6000, MEM=OUT411L  
// EXEC COFY2,FILE=20, LRECL=150, BLK=6000, MEM=OUT411U  
/\*  
//

C This JCL routine moves all source code files from mass  
C storage to the MVS 004 disk which can be accessed by  
C entering GET MVS then following the screen instructions  
C to move source files to your disk. If you want to move  
C the data files to MVS 004 then change the word SOURCE  
C to DATA in the JCL program below.

```
//JACK JOB (3266,0178) 'FASCHALL-2759',CLASS=A
//**MAIN ORG=NPGVM1.3266P
// EXEC PGM=IEBCOPY
//SYSPRINT DD SYSOUT=A
//FROM DD DISP=SHR,DSN=MSS.S3266.WFLOW.SOURCE
//INTO DD UNIT=3350,VOL=SER=MVS004,DISP=(NEW,KEEP),
//      SPACE=(CYL,(16,4,10),RLSE),DSN=S3266.SOURCE
//SYSUT3 DD UNIT=SYSDA,SPACE=(CYL,(2,2))
//SYSUT4 DD UNIT=SYSDA,SPACE=(CYL,(2,2))
//SYSIN DD *
   COPY OUTDD=INTC,INDD=FFCM
/*
//
```

## APPENDIX B

### LITERARY OF AIRFOIL SECTION GEOMETRIES

- 0 = user input section coordinate data
- 1 = flat plate data
- 2 = symmetrical wing (11% thickness at 30% chord)
- 3 = supercritical wing (cambered, 12% thickness at 32% chord)
- 4 = NACA 24-30-0 (cambered, 12% thickness at 30% chord)
- 5 = F-14 wing (cambered, 9.5% thickness at 37% chord)
- 6 = A-7 wing (7 deg droop at 20% chord, 7% thickness at 43% chord)
- 7 = LISSAMAN 7769 Airfoil (cambered, 11% thickness at 30% chord)
- 8 = NACA 0010 (symmetrical, 10% thickness at 30% chord)
- 9 = NACA 0010-34 (symmetrical, 10% thickness at 40% chord)
- 10 = NACA 0010-35 (symmetrical, 10% thickness at 50% chord)
- 11 = NACA 0010-64 (symmetrical, 10% thickness at 40% chord)
- 12 = NACA 0010-66 (symmetrical, 10% thickness at 60% chord)
- 13 = NACA 16-009 (symmetrical, 9% thickness at 50% chord)
- 14 = NACA 63-010 (symmetrical, 10% thickness at 35% chord)
- 15 = NACA 63A010 (symmetrical, 10% thickness at 35% chord)
- 16 = NACA 64-010 (symmetrical, 10% thickness at 40% chord)
- 17 = NACA 64A010 (symmetrical, 10% thickness at 40% chord)
- 18 = NACA 65-010 (symmetrical, 10% thickness at 40% chord)
- 19 = NACA 65A010 (symmetrical, 10% thickness at 40% chord)
- 20 = NACA 66-010 (symmetrical, 10% thickness at 45% chord)

## APPENDIX C

THIS APPENDIX PRESENTS A COMPLETE INPUT DATA SET INCLUDING THE JCL CARDS REQUIRED TO EXECUTE THE PROGRAM FL27

APPENDIX D

THIS APPENDIX PRESENTS THE FLO27 OUTPUT DATA PRODUCED FROM THE INPUT DATA OF THE PREVIOUS APPENDIX.

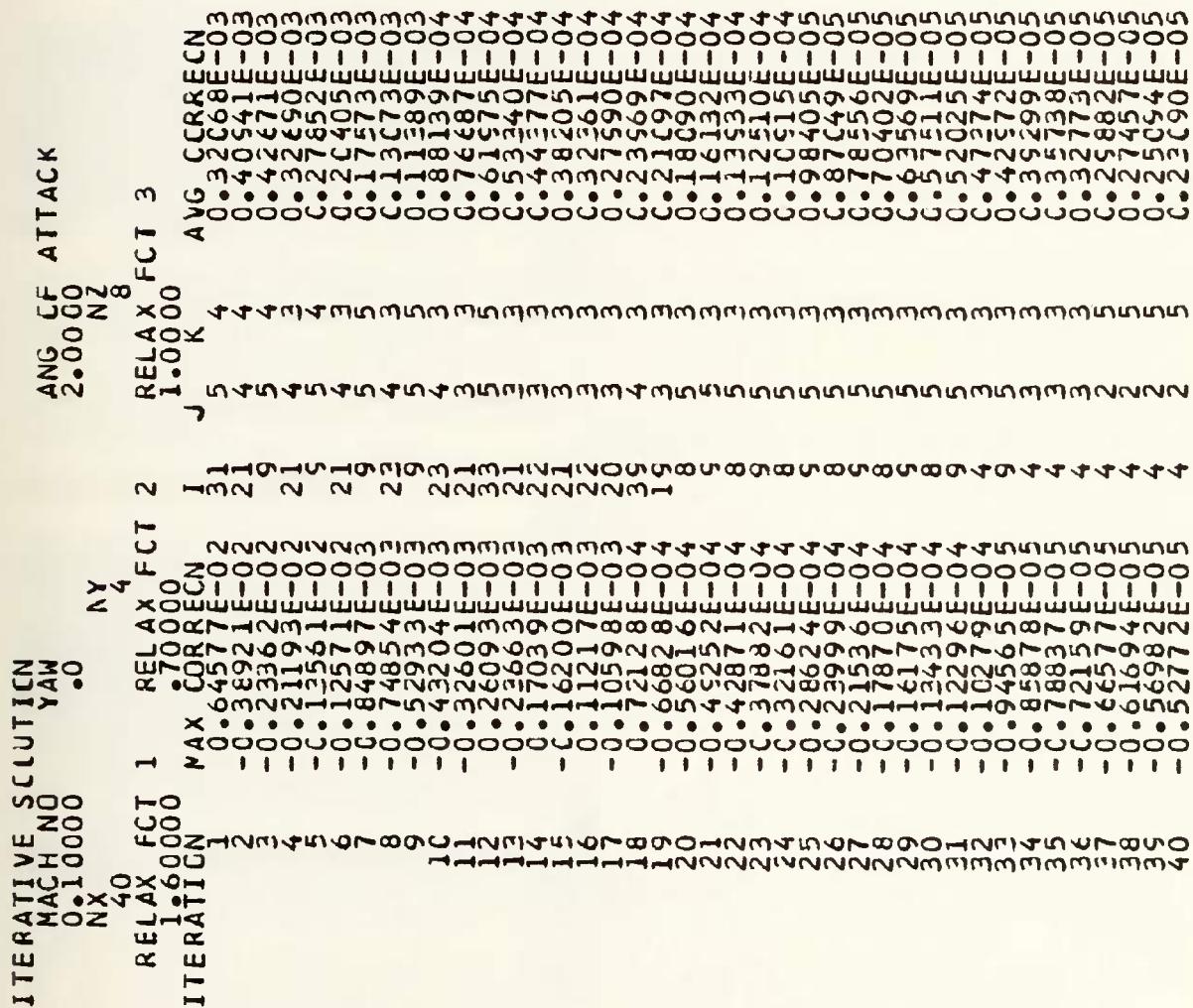
A46C MODIFIED FROM FILE 27 OF ANT CNY JAMESON CURRANT INSTITUTE THREE-DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING FINITE VOLUME SCHEME NACA 572 WING SECTION FUSELAGE RAE

SLEEP	32.3275	CIHED	0.0
PROFILE AT Z =		0.1E SLOPE	-0.0720
TE ANGLE	16.0833	X SING	0.0024
		Y SING	-0.0000

$$NL = 21, \quad XF(NL) = C_0$$

EXP. YP)

SECTION DEFINITION AT Z =		CHORD		THICKNESS RATIO	
X <sub>LE</sub>	Y <sub>LE</sub>	0.0	8.6000	1.0000	0.0
0.0	Y <sub>MIN</sub>	0.0	Y <sub>MAX</sub>	J <sub>MAX</sub>	YDIF
-4.220E-01	X <sub>LE</sub>	10	9.68750	7.880E-01	33
SECTION DEFINITION AT Z =		CHORD		THICKNESS RATIO	
6.1307	Y <sub>MIN</sub>	0.0	6.4500	1.0000	0.0
-4.220E-01	X <sub>LE</sub>	10	19.3750	7.880E-01	33
SECTION DEFINITION AT Z =		CHORD		THICKNESS RATIO	
12.2614	Y <sub>MIN</sub>	0.0	4.3000	1.0000	0.0
-4.220E-01	X <sub>LE</sub>	10	7880E-01	Y <sub>MAX</sub>	YDIF





## SECTION CHARACTERISTICS

MACH NO	YAW	ANG OF ATTACK
0.10000	•0	2.0000
SPAN STATION	CL	CM
0.0	•20238	•71088E-02
3.087499	•24033	•24623E-02
7.074599	•26515	•48115E-02
11.062498	•28127	•57074E-02
15.049998	•28695	•65491E-02
19.037497	•24168	•70588E-02

## WING CHARACTERISTICS

MACH NO	YAW	ANG OF ATTACK
0.10000	•0	2.0000
SPAN STATION	CD FORM	CD FRICTION
0.25575	-•32534E-02	•10000E-01
CM YAW	CM ROLL	CM PITCH
-0.00467	•23919	-•33140

## WING CHARACTERISTICS

MACH NO	YAW	ANG OF ATTACK
0.10000	•0	2.0000
SPAN STATION	CD FORM	CD FRICTION
0.25575	-•32534E-02	•67466E-02
CM YAW	CM ROLL	CM PITCH
-0.00467	•23919	-•33140

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## SECTION CHARACTERISTICS

MACH NO	YAW	ANG OF ATTACK
0.10000	0	2.0000
SPAN STATION	CL	CM
0.0	.22093	.18197E-01
1.93750	.24319	.53303E-02
3.87499	.26068	.144194E-C2
5.81249	.27508	.44517E-C5
7.74595	.28683	.72064E-03
9.68749	.29643	.11954E-C2
11.62499	.30359	.16262E-02
13.56248	.30863	.20637E-02
15.5998	.30746	.27385E-C2
17.43747	.29141	.41059E-02
19.37497	.21866	.42003E-02

## WING CHARACTERISTICS

MACH NO	YAW	ANG OF ATTACK
0.10000	0	2.0000
CL	CD FORM	CD
0.27663	.87151E-03	.10000E-01
CM YAW	.CM RCLL	CM PITCH
-0.00145	.25615	-.35963

## WING CHARACTERISTICS

MACH NO	YAW	ANG OF ATTACK
0.10000	0	2.0000
CL	CD FORM	CD
0.27663	.87151E-03	.10000E-01
CM YAW	.CM RCLL	CM PITCH
-0.00145	.25615	-.35963

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ITERATIVE SOLUTION  
 MACH NO 0  
 0.10000  
 NX 160  
 RELAX FCT 1  
 1.20000  
 ITERATION 1  
 MAX RESIDUAL 1  
 -0.1385E-C2  
 NY 16  
 RELAX FCT 2  
 1.00000  
 MAX CORRECN  
 0.95314E-03  
 -0.96428E-03  
 0.42692E-03  
 -0.24824E-03  
 -0.21125E-03  
 MAX RESIDUAL 1  
 -0.6224E-03

ANG OF ATTACK  
 2.00000  
 NZ 32  
 RELAX FCT 3  
 1.00000  
 MAX CORRECN  
 1.5  
 1.2  
 1.0  
 0.8  
 0.6  
 0.4  
 0.2  
 0.1  
 0.0  
 AVG CORRECN  
 0.20565E-04  
 0.12764E-04  
 0.096247E-05  
 0.079284E-05  
 0.071493E-05  
 WORK RELUCTN/CYCLE  
 4.00000

MAX RESIDUAL 1  
 -0.13855E-02  
 0.98673E-03  
 0.87373E-03  
 0.73407E-03  
 0.62240E-03  
 CONV TOLERANCE  
 0.8187 0.1000E-05

K 4  
2333

SECTION CHARACTERISTICS

ANG GF ATTACK

MACH NO	YAW	CL	CD	CM
0.0	0.0	2.25679	2.5222E-01	1.0517
0.9375	0.0	2.25693	1.3934E-01	1.0917
0.90625	0.0	2.26526	1.5353E-01	1.1244
0.84374	0.0	2.27275	1.5353E-01	1.1393
0.81249	0.0	2.27957	1.5466E-01	1.1684
0.78124	0.0	2.28574	1.5466E-01	1.1824
0.74999	0.0	2.29419	1.5050E-01	1.1944
0.71874	0.0	2.29633	1.4614E-01	1.2056
0.68749	0.0	2.30116	1.4614E-01	1.2147
0.65624	0.0	2.30527	1.4848E-01	1.2242
0.62499	0.0	2.30873	1.5050E-01	1.2276
0.59373	0.0	2.31151	1.5271E-01	1.2287
0.56248	0.0	2.31326	1.5466E-01	1.2335
0.53123	0.0	2.31355	1.5656E-01	1.2093
0.50098	0.0	2.31468	1.5656E-01	1.1776
0.46972	0.0	2.30555	1.6767E-01	1.1777
0.43747	0.0	2.29369	1.6767E-01	1.1777
0.40622	0.0	2.26619	1.9595E-01	1.2991
0.37497	0.0	2.20055	1.9595E-01	1.2991
0.34371	0.0	1.68273E-01		

WING CHARACTERISTICS

MACH NO	YAW	ANG GF ATTACK	CD	CM	L/D FORM
0.0000	0.0	2.0000	1.0000E-01	1.3832E-01	1.00
0.1000	0.0	CD FCRM	1.0000E-01	1.3832E-01	1.00
0.28117	0.0	3.8318E-02	CW ROLL	-0.36670	
0.00116	0.0	0.25975			

A46C MODIFIED FROM FLC27 OF ANTONY JAMESON CURRENT INSTILUTE THREE-DIMENSIONAL WING ANALYSIS IN TRANSonic FLOW USING FINITE VOLUME SCHEME BOEING VERSION 1 PREPARED BY DR. HAI-CHOW CHEN STANDARD Boeing INPUT FORMAT  
END OF CALCULATION



SPAN STATION = POINTS 1.93750  
NO. OF DATA = 101

SPAN NO.	STATION	CF DATA	POINTS	$\Sigma$
1	X/C	GP	X/C	101
1	C000000	C• 236239	C• 566	0• 811
0	846730	C• 102997	C• 029155	0• 672
0	706152	C• 029155		

X/C	CP
0.521777	0.161171
0.774854	0.059673
0.640641	0.027657
0	0







SPAN STATION = POINTS 7.749  
NO. OF DATA POINTS = 1

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 1  
 0

71 874 101 X 961 847 543 357 114 030 001  
0000000000000000

= FCINTS =  
 CP 10 8 7 6 5 4 3 2 1  
 C 23 31 10 8 7 3 8 6 1 2 9 1 1 6 9 4 7 3 1 2 4 1 4 8 0 5 6 9 7 2 4 6 3 0 6 8 0 2 3 5 6 9 2 4 2 0 9 6 1 2 4 5 2 3







460644846572044  
42313508648675726  
4252604206889175716  
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7156972028826192671  
7156972028826192671  
10m6m046m6m4m210  
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X/C 883 857  
X/C 740 077  
X/C 690 015  
X/C 385 015  
X/C 291 398  
X/C 134 502  
X/C 143 458  
X/C 148 326  
X/C 498 326  
X/C 003 563  
X/C 000 0363  
X/C 009 017  
X/C 028 618  
X/C 061 094  
X/C 011 048  
X/C 017 049  
X/C 145 933  
X/C 313 577  
X/C 546 485  
X/C 672 059  
X/C 810 059  
X/C 960 471



SPAN STATION = 18-40622  
NO. OF DATA POINTS = 101  
 $X/C$  CP  $X/C$  CP  $X/C$  CP  $X/C$  CP  
1.000000 0.224658 0.560494 0.155639 0.521779 0.149727 0.883859 0.11730  
0.846732 0.293051 0.810358 0.724755 0.7485 0.052997 0.740167 0.05583  
0.706153 0.025340 0.672999 0.023433 0.640643 0.026703 0.609078 0.02724



0.460619	-0.245829	0.488450	-0.239440	0.517072	-0.229495	0.546466	-0.21668
0.576693	-0.204904	0.607655	-0.186239	0.639467	-0.163669	0.672057	-0.14166
0.705396	-0.124829	0.739503	-0.112534	0.774369	-0.097547	0.810060	-0.07234
0.846512	-0.036530	0.883731	-0.006437	0.924712	-0.025749	0.960469	0.07570
1.000000	C.142642						

## APPENDIX E

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE POTENTIAL FLOW PROGRAM FLO27.

```
***** FLC27*****9/12/83*****  
*** THREE DIMENSIONAL WING ANALYSIS IN TRANSONIC FLOW USING  
*** FINITE VOLUME SCHEME WITH SHEARED PARABOLIC COORDINATES  
*** PROGRAMMED BY ANTHONY JAMESON, JANUARY-APRIL 1977  
***  
*** THE BEING VERSION OF FLO27 WAS PREPARED BY DR. HAI-CHOW  
CHEN, WITH THE FOLLOWING MODIFICATIONS:  
1) TEMPORARY STORAGE OF THE LARGE CORE MEMORY REQUIREMENTS  
HAS BEEN IMPLEMENTED TO REDUCE THE COMPUTING COSTS  
BY BUFFERING DATA IN AND OUT OF CORE.  
2) STANDARD BOEING INPUT FORMAT FOR THE WING SECTION  
HAS BEEN USED.  
3) SUBPROGRAM BLIN HAS BEEN IMPLEMENTED TO ADD THE  
DISPLACEMENT THICKNESS TO THE ORIGINAL WING SECTIONS  
4) WING SECTION LEADING EDGE SINGULAR POINT IS FOUND BY  
COMPUTING THE FOCUS OF A PARABOLA BY LEAST-SQUARE FIT CENTERED AT THE LEADING EDGE POINT.  
A IS SUPPLIED BY THE USER THROUGH INPUT CARD.  
5) TRAILING EDGE CLOSURE ANGLE AND BI-SECTOR SLOPE ARE  
COMPUTED BASED ON BACKWARD DIFFERENCE.  
6) OPTION FOR PRINTER-PLOTTING OF THE UNWRAPPED  
WING SECTIONS IS AVAILABLE  
*****  
THE FOLLOWING FILES ARE USED TO EXECUTE FLO27. SOME OF THESE  
FILES ARE USED SUBSEQUENTLY IN OTHER MODULES OF THE VISCOUS/  
INVIScid INTERACTIVE WING SYSTEM  
FILE1 IS USED TO BUFFER DATA IN AND OUT OF CORE  
FILE2 IS USED TO BUFFER DATA IN AND OUT OF CORE  
FILE3 IS USED TO BUFFER DATA IN AND OUT OF CORE
```

FILE4 IS USED TO READ IN THE VELOCITY POTENTIAL  
GENERATED PREVIOUSLY

FILE8 IS WRITTEN FOR DATA TRANSFER TO BEING  
TURBULENT BOUNDARY LAYER PROGRAM A411.

FILE5 IS USED TO SAVE SECTION SURFACE PRESSURE  
AGAINST X/C.

FILE10 IS USED TO SAVE THE SECTION X, Y, Z CORRESPONDING  
LOCATION FOR A411 IN WHICH CALCULATES THE DISPLACEMENT  
DISPLACEMENT THICKNESS WHERE X, Y, Z SHOULD BE THE WING SURFACE LOCATION  
FOR THE CURRENT RUN

FILE11 IS USED TO READ IN THE DISPLACEMENT  
THICKNESS FROM A411IN

FILE12 IS USED TO REPLACE PART OF THE INPUT CARDS  
BY CARD IMAGES

TAPE13 IS USED TO SAVE PART OF THE OUTPUT  
SKIPPED FROM THE LINE PRINTER

TAPE14 IS USED TO SAVE THE VELOCITY POTENTIAL  
FOR FUTURE USE

```
*****  
COMMON G(161,18,3),SO(161,35),VORT(115),ZV(115),  
1 IV(161,35),ITE1(35),ITE2(35),  
AO(161,18),BO(18),XO(35),YC(35),ZO(35),SCAL(35),  
NX,NY,NZ,KTE1,KTE2,ISYN,KSYN,FUS,N  
2 YAH,CYAH,SYAW,ALPHA,CA,SA,FNACH,N1,N2,N3,I0  
3 COMMON /OPPF/NL  
4 COMMON /PCKR/ PTCK  
COMMON /FLOR/ PI,P21,P31,FRES,IRESJRES,CG,IG,JG,KG,AG,NSUP  
COMMON /PARMT3/ XT3(161),YT3(161),ZT3(161),  
1 COMMON /PRS/ XOCO(161,11),YS(161,11),ZS(11),YLE(11),  
DIMENSION XS(161,11),TRAIL(11),NP(11),E1(11),E2(11),E3(11),  
2 SLOFT(11),D2(161),D3(161),SN(161),  
3 D1(161),D2(161),D3(161),XP(161),YP(161),  
4 SYPO(161),SM(161),CP(161),XMAX(35),YMAX(35),  
5 CHORD(35),ZPO(35),SCL(35),SCD(35),SCM(35),  
FIT(3),COV(3),P10(3),P20(3),TITLE(20),  
1 RES(20),CCUNT(201),P1MAP(3),FSMCU(3),
```



```

DO 12 NM=1, NME SH
C** INITIALIZE INPUT PARAMETERS WHICH HAVE RECOMMENDED PROGRAM VALUES ***
C**
C** P2 C(NM) = 0.7
C** P3 C(NM) = 1.0
C** FS MCO{NM} = 0.0
C** PT MAP{NM} = 0.0

C**
C** **** READ {5,510) FIT(NM), CCVO(NM), PIO(NM)
C** **** READ {5,501) FMACH, YAS AL, CDO
C** **** CALL GECH (ND, NS, NP, XS, YS, ZS, XLE, YLE, SLOP, TRAIL, XP, YP,
C** **** 12 AL PHA = AL/RAD
C** **** IF (BL, CF = AL/E0.1 GO TO 44
C** **** IF (PTCK = GE0.1 WRITE(6,600)
C** **** READ (11) TITLE(I), I=1,8), FMACH, ALPH A, NS
C** **** DO 40 K = 1, NS
C** **** READ (11) NFCK
C** **** NP CK1 = NP CK + 1
C** **** READ (11) (DUMX(NP CK1-I), DUMZ, DUMY (NP CK1-I), DELR(NP CK1-I),
C** 1 IF (PTCK = LE0.1 WRITE(6,600)
C** **** WRITE (6,52) K, NP CK, NP CK1
C** **** WRITE (6,54) (DUMX(NP CK1-I), DUMZ, DUMY (NP CK1-I),
C** **** 1 WRITE (6,54) (FELR(NP CK1-I), I=1, NP CK)
C** 3C CONTINUE (XS(1,K), YS(1,K), I=1, NP CK)
C** CALL BLIN (XS(1,K), YS(1,K), DELR, WEIG, NP CK, NL)
C** 4C CONTINUE
C** 44 CONTINUE
C** IF (PTCK = LT. 0.) GO TO 56
C** IF (PTCK = GE0.1 WRITE(6,600)
C** WRITE (10) (TITLE(I), I=1,8), FMACH, ALPH A, NS
C** DO 48 K = 1, NS
C** NP CK = AP{K}
C** NP CK1 = NP CK + 1
C** DO 48 I = 1, NP CK
C** DUMX(NFCK1-I) = XS(I,K) + XLE(K)
C** DUMY(NFCK1-I) = YS(I,K) + YLE(K)
C** 48 CONTINUE
C** WRITE (10) NP CK
C** WRITE (10) (DUMX(I), ZS(K), DUMY (I), I=1, NFCK)
C** IF (PTCK = LE0.1 GO TO 49

```

```

      WRITE(6,52) K,NPC,K1,ZSI(K)
      WRITE(6,54) (DUMX(I),ZSI(K),DUMY(I),I=1,NPCK)
5C CONTINUE
5C ENDFILE 10
52 FORMAT(1H0,5X,3I5,F11.4/)
54 CONTINUE (12F11.4)
      IF(KSYR.NE.0) YA = 0.
      ISYN = ISYN
      IF(YAL.NE.0) ISYN = 0
      YAW = YA/RAD
      CYAH = COS(YAW)
      SYAH = SIN(YAW)
      CA = CYAH*COS(ALPHA)
      SA = CYAH*SIN(ALPHA)
      IF(FCCT.LT.1.) GCTC91
      READ(4) NX,NY,NZ,NM,K1,K2,NIT
      MX = NX+1
      MY = NY+2
      MZ = NZ+3
      DO 62 K=1,MZ
      READ(4)((G(I,J,1),I=1,MX),J=1,NY)
      BUFFER(CLT(N3,1),(G(I,1,1),I=1,MX),J=1,NY)
      WRITE(N3,(G(I,J,1),I=1,MX),J=1,NY)
      IF(LUN(N3).GT.0.) GO TO 1
      BUFFER(CLT(N1,1),(G(I,1,1),I=1,MX),J=1,NY)
      WRITE(N1,(G(I,J,1),I=1,MX),J=1,NY)
      IF(LUN(N1).GT.0.) GO TO 1
      REAC(4) (VORT(K),K=K1,K2)
      REWIND N3
      REWIND N1
      91 CALL CCERD(NX,NY,NZ,KSYM,ZTIP,XLIM,ZLM,
      C      SY,AX,AZ,PZ,AC,BG,ZO)
      1 CALL SINGL(NS,NZ,KSYM,KTE1,KTE2,FUS,CHCRDO,ZS,XLE,YLE,
      C      SWEEP,DIHED,XO,YO,ZO,YFO,ZFCIE1,IE2,E3,IND)
      1 CALL SUFF(ND,RE,XFEO,XLIM,FX,NPXS,YS,IE2,KTE2,
      C      AO,XO,ZC,SO,SCAL2,V,IV,IE1,IE2,
      2 CALL ESTIM(XP,SN,D1,D2,D3,IND)
      3 IF((INC*EC.C) .GE. 1.) GO TO 101
      NM = 0
      NIT = 0
      CALL ESTIM(GC,TC291)
      IF((IG*EC.O) GO TO 1

```

```

RE WIND N2
RE WIND N2
101 IF (PTCK .GE. 1.0) WRITE (6,600)
      COV = 0.0
      COV = COVC(NM)
      COV = P10(NM)
      COV = P20(NM)
      COV = P30(NM)
      COV = FIT(NM) + NIT
      KIT = KIT(LT=2) KIT=2
      JI1 = NIT
      JRES = 0
      MRES = -NIT -21/200 +2
      NRRES = 0
      NX = NX +1
      NY = NY +2
      NZ = NZ +3
      KY = NY +1
      K1 = NZ +1
      K2 = NZ +1
      K1 = (KSYM.EC.O) GC TC 103
      K2 = NZ /2 +3
      K2 = NZ /2 +1
      K2 = NZ /2 +3
      IF (PTCK .LE. 0.) LZ = 3
      IF (PTCK .GT. 0.) LZ = 3
      WRITE (6,104)
      WRITE (49H0) INDICATIION OF LOCATION OF WING AND VORTEX SHEET,
      27H IN CORDINATE PLANE Y = 0.0
      27H ON (V(I,K),K=K1,K2), I=1,NX)
      DO 106 I=1,NX
      106 WRITE (6,65C) (V(I,K),K=K1,K2)
      108 CONTINUE
      IMAP = FTMAP(NM)
      IF (IMAP .NE. 0) GC TC 830
      WRITE (6,600)
      WRITE (6,112)
      112 FORMAT (49H0)H AND MAPPED SURFACE COORDINATES AT CENTER LINE AND TIP)
      1 DO 820 1SEC = LZKTE2(IMAP)
      1 WRITE (6,812) 1SEC ,ZP0(1SEC)
      812 FORMAT (15H0,1 12,3X,2 =,61-4) X ,20H SECTION PROFILE NO.,,
      820 CALL PXY (2,NX,A0,S0(1,1SEC))
      830 CONTINUE
      IF (PTCK .LE. 0.) GC TC 130
      WRITE (6,112)

```

```

116 FORMAT(15H0 TE LOCATION ,15H PCWER LAW )
117 WRITE(6,610) XLIM,AX
118 WRITE(6,600)
119 WRITE(6,118)
120 FORMAT(4CHNORMAL CELL DISTRIBUTION IN SQUARE ROUT PLANE/
121 15H0 Y
122 DO 120 KY=1,KY
123 WRITE(6,610) BC(J)
124 WRITE(6,122) SCALE FACTOR,15H PCWER LAW )
125 WRITE(6,610) SY,A,Y
126 WRITE(6,124) FOMAT(45HSPANWISE CELL DISTRIBUTION AND SINGULAR LINE/
127 15H X SING ,15H Y SING )
128 WRITE(6,128) Z0(K),X0(K),Y0(K)
129 WRITE(6,128) TIP LOCATION,15H PCWER LAW )
130 WRITE(6,610) ZLIM,AZ
131 CONTINUE
132 WRITE(6,600)
133 WRITE(6,132)
134 FORMAT(15H0 ITERATIVE SCLUTION)
135 WRITE(6,610) MACH NO
136 WRITE(6,134) MACH,YA,AL ,15H YAW
137 WRITE(6,610) FMACH,YA,AL ,15H YAW
138 WRITE(6,135) NX,NY,NZ ,15H NY
139 WRITE(6,640) NX,NY,NZ ,15H NZ
140 FORMAT(15H0 RELAX FCT 1 15H RELAX FCT 2 ,15H RELAX FCT 3 )
141 WRITE(6,610) P10(NM),P20(NM),P30(NM)
142 FORMAT(15H0 ITERATION,
143 15H MAX CORRECN ,4H J '4H K ;15H AVG CORRECN ;
144 15H MAX RESIDAL ,4H J '4H K ;15H AVG RESIDAL ;
145 12F CIRCULATION,15H SONIC P(S)
146 NIT = NIT +1
147 JIT = JIT +1
148 CALL MIXFLG
149 IF (IO.FC.O) GO TO 151
150 REWIND N1
151 REWIND N2
152 N1 = N2
153 N2 = N3

```

```

N3 = N
WRITE (6,66C) NIT, DG, IG, JG, KG, AG, FRES, IFES, JRES, KRES, ARES,
      1 LRES = LRES
      1 IF (LRES.EQ.0.MRES) LRES = 1
      1 IF (LRES.NE.1) GO TO 143
      1 NRES = NRES + 1
      1 COUNT (NRES) = NRES - 1
      1 RES = FRE
      1 IF (NM.LE.1) OR. NM.LT. MMESH) GO TO 251
      1 IF (ABS(EG).LE. CGV) GO TO 251
148 CONTINUE
      1 IF (NI.LT.MIT.AND.ABS(DG).GT.COV.AND.ABS(DG).LT.10.) GO TO 141
      1 GO TO 141
151 IF (JO.EG.1) GO TO 1
      1 REIND A1
      1 REIND A2
      1 JO = 1
      1 N3 = N2
      1 N2 = N1
      1 N1 = N
      1 GO TO 141
      1 RATE = 0
      1 IF (NRES.GT.1) RATE = (#(1./((COUNT(NRES)-COUNT(1))) )
      1 WRITE (6,162)
      1 FORMAT (15H MAX RESIDUAL,15H MAX RESILAI,15H
      1 15H REDUCTION/CYCLE,15H CONV TOLERENCE)
      1 WRITE (6,670) RES(1),RES(NRES),COUNT(NRES),RATE
      1 CGV
      1 WRITE (6,600)
      1 DO 164 F=1,3
      1 BUFFER IN (N1,1) ( G(1,1,M) G(M,1,M))
      1 READ (N1,ERR=151) (G(1,J,M) G(M,J,M)) J=1,MY
      1 IF (UNIT(N1).GT.0.) GO TO 151
      1 CONTINUE
      1 LX = NX/2 + 1
      1 K = 2
      1 KKK = 0
      1 C WRITE HEADER ON TAPE 8
      1 IF (NM.LT.MMESH) GO TO 17C
      1 REIND E
      1 REIND S
      1 NRC = KTE2 -(TITLE(I),I=1,8),FMACH,ALPHA,NRC
      1 WRITE (6,164)
17C CONTINUE

```

```

171 K = K * EC * MZ GO TO 191
IF (K .EQ. MY) DO 172
DO 172 J=1,MY
G(1,J,1) = G(1,J,2)
G(1,J,2) = G(1,J,3)
172 BUFFER IN (N1) (ERR=151) ((G(1,J,3)) (G(1,J,3))=1,MY)
READ (N1) (N1) (G(1,J,3)) (G(1,J,3))=1,MY
IF (UNIT(N1).GT.0) GO TO 151
IF (K*LL1*KTE1*OR1*K*GT*KTE2) GO TO 171
CALL VELQ ((K*SV*SM,CP,XP,YP,XMAX(K),XMIN(K),YMAX(K),YMIN(K))
11 I1 = ITE1(K)
12 CHCRO(K) = XP(I1) - XP(ILX)
CALL FCRCF (I1,I2) XP(YP(CP,AL) CHORE(K),XO(K),YPO(K),
1 KK = KKK +1
IF (KPLECT.GT.1 .AND. K.GT.KTE1) GC TO 185
IF (KPLECT.EQ.0 .AND. KKK .GT. 1) GO TO 185
WRITE (E'000)
WRITE (E'182)
FORMAT (24H0SECTION CHARACTERISTICS/
15H NO. MACH NO. 15H YAW
1 WRITE (E'610) FMACH,YA,AL ,15H ANG OF ATT
1 WRITE (E'184)
184 FORMAT (12HOSSPAN STATIC ) 15H CL ,15H CD
1 WRITE (15H CM )
185 WRITE (E'610) ZPO(K),SCL(K),SCM(K)
2 = ZPC(K)
IF (INIT.LE.0) GC TO 850
IF (KPLECT.LE.2) CALL CPLOT (2,NX,FACH,XP,YF,CP,SM,11,I2,KPLO
850 CONTINUE
C IF (NM.LT.NCI) WRITE CNE FILE ON TAPE 8
1 WRITE (E'NCI) NMESH,GO TO 186
1 WRITE (E') (XT3(1),ZT3(1),YT3(1),UT3(1),WT3(1),VT3(1),I=1,NCI)
NR C=I2-1+1
WRITE CP VS X/C SECTION DATA FCR FINAL MESH ON TAPE 9
1 WRITE (E'900) ZPO(K)
1 WRITE (E'910) NRD
1 WRITE (E'920) XQC D(J) CP(J) J=11,12
1 WRITE (E'14HS PAN STAT ION = F12.5
1 FORMAT (1X,20HNC,CF DATA POINTS = 15)
1 FORMAT (1X,6H,X/C,8X,2HCP,7X,3HX/C,8X,2HCF,7X,3HX/C,8X,2HCP
C 17X,3HX/C,8X,2HCF,3X)
95C FORMAT (E'F10.6)
186 CONTINUE

```

C WHEN KPLOT = 2 CALL SUBROUTINE VERTEC WHICH PLOTS CP VS X/C  
 C FOR EACH SECTION OF THE FINAL MESH

```

1 IF ((KPLCT.EQ.2 .AND. NM.EQ.MMESH)) CALL VERTEC(1,12,XOCD,CP,NRD)
   GO TO 171
191 CONTINUE
  IF (NM.EQ.1 .AND. MMESH) GO 171
  END FILE 8
  REWIND 6
  ENDFILE 6
  REWIND 5
  REWIND 5
200C CONTINUE
  CALL TCTFOR (KTE1,KTE2,CHORD,SCL,SCD,SCM,XC,YPO,ZPO,
    1 CD1      CL,CD1,CMR,CMY.)
    CD      CYA,CD1
    CD      = CDO + CD1
    VLC      = 0
    IF (ABS(CD1).GT.1.E-6) VLD1 = CL/CC1
    VLC      = 0
    IF (ABS(CD1).GT.1.E-6) VLD = CL/CD
    WRITE (6,600)
    WRITE (6,192)
    FORMAT (21HOKING CHARACTERISTICS/
    15H      MACH NO ,15H YAW
    15H      FMACH,YA,AL
    WRITE (6,610)
    WRITE (6,194)
    FORMAT (15H      CL
    15H      CD,CD1,CC0,CD,VLD1,VLC
    15H      CM YAW,15H CM RCLL
    WRITE (6,610) CMY,CMR,CMP
    REWIND 5
    IF ((KPLCT.EQ.1)) GO TO 201
    CALL RPLCT(IPLCT,NRES,COUNT,TITLE,FMACH,YA,AL,NX,NY,NZ)
    CALL DRAW (IPLCT,XMAX,YMAX,XMIN,YMIN,ZPOFUS,TITLE,NZ,KTE1,KTE2)
    CALL TFREED (IPLCT,SV,SM,CP,XP,ZPOFILE,151,CD,CHORD0,XSCAL,PSCAL)
    1 IF ((IO.EQ.0)) GO TO 151
    IF ((NX.EQ.1)) GO TO 201
    GO TO 1
203 CONTINUE
    NX      = NX
    NY      = NY
    NZ      = NZ
  
```

```

CALL CCCRD (NX,NY,NZ,KSYM,ZTIP AZ,BG,ZO) 1
1 CALL SINGL (NS,NZ,KSYH,KTE1,E2,FUS,ZC,YFC,ZPC,E1,E2,E3,IND)
1 CALL SUFF (ND,NE,NS,NX,E0,DIH,XO,YO,ZS,XLE,YLE)
1 YAW,XTE0,XLIM,ISY,M,KSYM,KTE1,ZS,ITE1,SLOPf,TRAIL,
1 AO,XO,ZO,SO,SCAL,ZV,IV,ITE1,ITE2,
1 XP,YP,SN,C1,D2,D3,IND,
1 IF (INC.EQ.0) GC f C 291
1 IF (IO.EQ.0) GO TO 221
1 CALL REFIN
1 RE WIND N1
1 RE WIND N2 = FSMCC(NM)
1 IF (NSMCC.LT.1,NSMCC
1 DO 202 N=1,NSMCC
1 CALL SMC C
1 IF (IO.EQ.0) GO TO 221
1 RE WIND N1
1 RE WIND N2 = N1
1 N1 = N2
1 N2 = N3
1 N3 = NM +1
1 NM = 0
1 NIT
1 GO TO 1C1 = NX/2
1 NY = NZ/2
1 NZ = NZ/2
1 CALL CCCRD (NY,AZ,KSYM,ZTIP AZ,BG,ZO)
1 CALL SINGL (NS,NZ,KSYH,KTE1,E2,FUS,ZC,YFC,ZPC,E1,E2,E3,IND)
1 CALL SUFF (ND,NE,NS,NX,E0,DIH,XO,YO,ZS,XLE,YLE)
1 YAW,XTE0,XLIM,ISY,M,KSYM,KTE1,ZS,ITE1,SLOPf,TRAIL,
1 AO,XO,ZO,SO,SCAL,ZV,IV,ITE1,ITE2,
1 XP,YP,SN,C1,D2,D3,IND,
1 IF (INC.EQ.0) GC f C 291
1 GO TO 1E1
202 221 NX
221 NY
221 NZ
221 K1 = KTE1
221 K2 = KTE2
221 WRITE (14) NX,NY,NZ,NW,K1,K2,NIT
221 DO 262 K=1,N1 (G(1,1,1) (G(1,1,1) G(MX,MY,1))
221 EUEFER IN {N1,1} (N1,1) (G(1,1,1) (G(1,1,1) G(MX,MY,1))
221 READ (N1,ERR=281) (G(1,1,1) (G(1,1,1) G(1,1,1)) J=1,MX),J=1,MY
221 IF (UNI(N1) (G(1,1,1) (G(1,1,1) G(1,1,1)) J=1,MX),J=1,MY)
251 262 WRITE (14) (G(1,1,1) (G(1,1,1) G(1,1,1)) J=1,MX),J=1,MY

```

```

REWIND ^1
WRITE (14) (VORT(K),K=K1,K2)
ENDFILE 14
REWIND 14
CALL SPLIT(1,1STOP)
IF (1$TCF.EC1) GO TO 161
YI T IF (INIT.LT.MIT.AND.ABS(DG).GT.COV.AND.ABS(DG).LT.10.) GC TO 141
GO TO 161
REWIND 4
GO TO 151
281 WRITE (6,6000)
291 WRITE (6,292)
292 FORMAT (24HOBAD DATA,SPLINE FAILURE)
GO TO 1
301 CONTINUE
REWIND 10
REWIND 11
IF (KPLC).GT.0 CALL PLOT(0.,0.,955)
STCP
50C FORMAT (1X)
51C FORMAT (8F10.6)
53C FORMAT (2CA4)
60C FORMAT (1H1)
61C FORMAT (F12.5,7G15.5)
63C FORMAT (1HO,20A4)
64C FORMAT (1X,7I15)
65C FORMAT (1I0,7I13)
66C FORMAT (1I0,7I15,5,2E15.4,3I4,E15.5,F10.5,I10,F10.3)
67C FORMAT (2E15.4,2F15.4,E15.4)
END

```

```

C**SUBROUTINE BLIN*****
SUBROUTINE BLIN (XT,YT,DELR,WEIG,N,AL)
CCCCCCCCCCCCCCCC
      SUBPROGRAM FOR NORMALLY ADDING THE DISPLACEMENT
      THICKNESS TO THE ORIGINAL WING SECTIONS
      XT :  CONTAIN THE X COORDINATES OF THE ORIGINAL
             WING SECTION WHEN CALLED
      XT :  CONTAIN THE X COORDINATES OF THE DISPLACED
             WING SECTION ON RETURN
      YT :  CONTAIN THE Y COORDINATES OF THE ORIGINAL
             WING SECTION WHEN CALLED
      YT :  CONTAIN THE Y COORDINATES OF THE DISPLACED
             WING SECTION ON RETURN
      DELR:  THE DISPLACEMENT THICKNESS
      COMMON /FCKR/ PTCK
      DIMENS(1N XT(1),YT(1),DELR(1))
      WRITE(6,1000)
1000 I = 1
      X2 = XT(I)
      Y2 = YT(I)
      20 C IF ((I .EQ. 1) .OR. X2 .EQ. 0.0) GO TO 300
      Y3 = YT(I+1)
      30 C IF ((I .NE. 1) .AND. X2 .EQ. 0.0) GO TO 400
      X1 = 2.0*X2 - X3
      Y1 = 2.0*Y2 - Y3
      40 C IF ((I .NE. N) .AND. X1 .EQ. 0.0) GO TO 500
      X3 = 2.0*X2 - X1
      Y3 = 2.0*Y2 - Y1
      50 C CONTINUE
      X12 = X1 - X2
      X23 = X2 - X3
      X31 = X3 - X1
      IF (ABS(X31) .LE. 1.0E-6) GO TO 600
      DX = (X31*(X12*X31))*.Y1
      DYX = DX + (X12-X31)*(X12*X23)*Y2
      DDX = DX + X12/(X31*X23)*Y3
      IF (ABS(DYX) .LE. 1.0E-6) GO TO 820
      DX = -1.0/DYX
      GO TO 700
      60 C DDX = 0.0
      70 C CONTINUE
      IF ((I .NE. N)) GO TO 880
      800 CONTINUE
      SI = 1.

```

```

IF (I•LT•NL) SI = -1.
GO TO 650
CONTINUE
S = 0
DL = DELR(I)
DX = DL+SI
GO TO 1000
850 CONTINUE
S = SQRT(S)
S = 1./S
F = (DX*XN*S*SI.LT.0.) F = -1.
IF (DL = S*F
DX = ABS(DX*XN)*S*SI
DX = DX*CL
DX = DY*DL
XT(I) = X2 + DX*WEIG
YT(I) = Y2 + DY*WEIG
880 CONTINUE
IF (PTCK(iLE, 1, ) GO TO 890
WEITE(C,IC00, I,F,S,DL,DY,DY,XN,XT(I),YT(I),CYX,WEIG
890 CONTINUE
IF (I•EC.N) GO TO 900
X1 = X2
Y1 = Y2
X2 = X3
Y2 = Y3
I = I+1
GO TO 200
900 RETURN
1000 FORMAT (1H ,15,F7.2,9G13.5)
END

```

```
C**SUBROUTINE PPXY*****PPXV (I1,I2,X,Y)
```

```
C SUBPROGRAM FOR LINE PRINTER PLOTTING OF THE UNWRAPPED
```

```
WING SECTIONS
```

```
COMMON /PCCKR/ TICK
COMMON /SHARE/ LINE(100)
DIMENS(X(1),Y(1))
DATA IB/1H/,IP/1H+/,KMAX/100/,ACC/1.5/,I2/1H+/,ICONST/0/
1 DO 10 I=1,100
LINE(I)=IB
10 CONTINUE
1C YMAX=-1.0E35
YMIN=-YMAX
WICTH=KMAX-5
DO 20 I=1,12
YMAX=AMAX(YMAX,Y(I))
YMIN=AMIN(YMIN,Y(I))
2C CONTINUE
VAL=AES(YMAX)+ABS(YMIN)
S=WICTH/VAL
KK=0
IF (ICONST.LE.0) LINE(KK)=12
IF (KK.NE.0) LINE(KK)=12
DO 30 I=1,12
K=S*(YMAX-Y(I))+ADD
IF (K.LT.1) K=1
IF (K.GT.KMAX) K=KMAX
LINE(K)=IP
WRITE(6,100) I,X(I),Y(I),LINE
LINE(K)=18
IF (K.EQ.KK) LINE(KK)=12
30 RETURN
10C FORMAT (1X,I3,2F10.4,4X,100A1)
END
```

C\*\*\*SUBROUTINE LSQR\*\*\*\*\*LSQR (NL,NB,XP,YP,XSING,YSING)

SUBPROGRAM FOR WING SECTION LEADING EDGE SINGULAR POINT  
CALCULATION BY MEANS OF COMPUTING THE FOCUS OF A  
PARABOLA BY NB \* Z+ POINTS LEAST-SQUARE FIT CENTERED AT  
THE LEADING EDGE

NB : SUPPLY BY THE CALLING PROGRAM GEOM

```

COMMON /FCKR/ PTCK
DIMENSION XP(1),YP(1)
N1 = NL - NB
N2 = NL + NB
N3 = N2 - N1 + 1
A1 = N0
B1 = N0
C1 = N0
A2 = N0
B2 = N0
C2 = N0
A3 = N0
B3 = N0
C3 = N0
D1 = N0
D2 = N0
D3 = N0
SCALE = 100.
SCALE2 = 50.
DO 300 I = NI , N2
YY = (YP(I) - YP(NI))*SCALE
B1 = B1 + YY
YP2 = YY + YY
C1 = C1 + YF2
YF3 = YF2 * YY
C2 = C2 + YP3
YF4 = YF2 * YY
C3 = C3 + YF4
XX = XP(I)*SCALE2
C1 = D1 + XX
YY = YY + XX
D2 = D2 + XX
Y2X = YF2 + Y2X
300 D3 = D1
A2 = B1
B2 = C1
A3 = C2
B3 = C2

```

```

FA1 = B2*C3 - B3*C2
FA2 = A2*B3 - A3*B2
DEI = A1*FA1 + B1*FA2 + C1 *FA3
DI = 1 *FA1*C1
FA1 = FA2*D1 - B1*(C3)*D1
FA2 = (E3*C1 - A2*C3)*D1
FB1 = (A1*D1 - A1*B3)*D1
FB2 = (A1*D1 - E2*(C1))*D1
FC1 = (A1*B2 - A1*C2)*D1
FC2 = (A1*C1 + FB2*D2 + FC1*D3
FC3 = FA1*D1 + FB3*D2 + FC3*D3
AB = FA2*C1 + FB3*C1
BC = B*SCALE**2
CC = C*SCALE**2
A = A/SCALE**2
B = B/SCALE**2
C = C/SCALE**2
XSING = A + (1 - E**2)*25/C
YPT = -B* .5/C + YP(NL)
IF (PT < 0) N = 0.1 GO TO 520
WR1TE((C*400)5X 'LEAST SQUARE MATRIX FOR LEADING EDGE',
400 FORMAT(1H0$'LEAST-SQUARE FIT',/
1 WRITE((C*500)1 A1,B1,C1,D1
1 WRITE((C*500)1 A2,B2,C2,D2
1 WRITE((C*500)1 A3,B3,C3,D3
1 WRITE((C*500)1 FA1,B1,F1,C1
1 WRITE((C*500)1 FA2,B2,F2,C2
1 WRITE((C*500)1 FA3,B3,F3,C3
1 WRITEN((C*500)1 X$ING,Y$ING,A,B,C,DET,DI
500 FORMAT(1H0G13.5)
520 CONTINUE
DXAM = C.
DXZN = C.
DO 650 I = N1 YP(NL)
Y = YP(I) - Y + C*Y**2
X = A + B*Y + XP(I)
DX = X - XP(I)
DX2 = CX*DX
R2 = R2 + DX2
DXA = ABS(DXA)
IF (DXA.GE.DXA) GC TO 600

```

```

DXAM = CXA
DX2M = CXAM**2
CONTINUE
IF (PTCK .LE. 0.) GC TC 65C
WRITE(6,70) I,X,Y,DX,DX2,R2,CXAM,DX2M,XP(1),YP(1)
70C CONTINUE
IF (PTCK .LE. 0.) GC TC 75C
RA = R2/A1
WRITE(6,70) N'RA',DXA
75C FORMAT(113.9G13.5)
CONTINUE
RETURN
ENTRY LSC
IF (DXA .LE. -E-4) RETURN
WRITE(6,80) DXAM
80C FORMAT(1F0.5X,'WARNING ?? DEVIATION OF THE LEADING POINTS',
1      ' FROM PARABOLA IS GREATER THAN 0.C001',DXA,'.CXAM = ',G13.4),
      RETURN
END

```

```

C** SUBROUTINE GEOM*****SUBROUTINE GEOM (NDINS,NP,XS,YS,ZS,XLE,YLE,SLOP,TRAIL,XP,YP,
      FUS,XTEO,CHGRD,ZTIP,SWEET,DIHED,
      FIX,PX,PZ,ISYNO,KSYN)

```

GEOMETRIC DEFINITION OF WING

STANDARD BOEING INPUT FORMAT FOR WING SECTION DATA IS USED  
OPTION FOR WING SECTION TRAILING EDGE CLOSURE ANGLE  
AND BISECTOR SLEP BE AUTOMATIC COMPUTED IS AVAILABLE  
LEADING EDGE SINGULAR POINT CAN BE AUTOMATIC COMPUTED  
BY INVOKING THE OPTION TO CALL LSQR

```

COMMON /PCKR/  PICK
COMMON /EFF/  NL
DIMENS(1)  XS(ND,1),YS(ND,1),ZS(ND,1),XLE(1),YLE(1),
1           SLOPT(1),TRAIL(1),XP(ND),YP(ND),NP(1)
C*** INITIALIZING INPUT PARAMETERS WHICH HAVE RECOMMENDED PROGRAM VALUES ***
C*** FNB = 2.0
      PX = 0.0
      PZ = 0.0
      FIX = 0.0
      TRL = 0.0
      SLTING = 0.0
      XSYING = 0.0
      YSYING = 0.0
      ZSYM = 0.0
RAD = 57.295779513082
READ (E,501)
READ (E,510) ZSYM,FNS,SWEEP,DIHED,FUS
IF (FNS.EQ.3) RETURN
KSYM = ZSYM
IF (FUS.EQ.0) KSYM = 1
NS = FNS
WR ITE (E,2)
2 FORMAT (15F0) FUELAGE RAD )
      WRITE (E,10) FLS
      WRITE (E,4)
      4 FORMAT (15H0) SWEEP DIHED ,15H
      WRITE (E,10) SWEEP/RAD
      SWEEP = DIHED/RAD
      DIHED =

```



```

CA = COS(ALPHA)
SA = SIN(ALPHA)
DO 22 I=1,N
XS(I,K) = SCALE*((XP(I)-XX)*CA + THICK*(YP(I)-YY)*SA)
YS(I,K) = SCALE*(THICK*(YP(I)-YY)*CA - (XP(I)-XX)*SA)
32 SLOP(K) = THICK*SLT - TAN(ALPHA)
TRAIL(K) = N
NP(K) = THICK*TRL/RAD
CHORDO = AMAX1(CHORD,ALPHA*NE*0.) ISYMC = C
IF (YS YP LE 0.0 CR. ALPHA*NE*0.) ISYMC = C
WRITE(6,42) ZS(K)
FORMAT(2,15H0 SECTION XLE,15H 15H
42 1 15H THICKNESS RATIO,15H 15H
2 WRITE(6,610) XL,YL,CHRD,THICK,AL
YMIN = YP(NL)
YMAX = YMIN
DO 44 I=1,N
IF (YP(I) .GE. YMIN) GO TO 43
JMIN = IF(I)
YMIN = IF(I)
IF (YP(I) .LE. YMAX) GO TO 44
43 JMAX = IF(I)
YMAX = YP(I)
YDIF = YMAX - YMINT
NN = N - 1
SUM = C.
DO 46 I = NL,NN
SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
CONTINUE
46 NM = NL - 1
DO 48 I = 1,NM
SUM = SUM + .5*(YP(I)+YP(I+1))*(XP(I+1)-XP(I))
CONTINUE
48 NM = NL - 1
FORMAT(6,15H0 YMIN,15H YCIF,15H AREA
30C 1 15H MAX YMIN,15H YMAX,15H SUM
FORMAT(6,320) G12.4,III,G19.4,I11,G15.4
CALL LS
IF (FUS*LE*C.) GO TO 61
R = AMAX1(0.0,FLS*#2-YLE(1)*#2)
Z = ZS(K) - 2*S1+SQRT(R)
R = FUS*#2/(YLE(K)*#2+Z*#2)
ZS(K) = Z*(1.0,-R)
YLE(K) = YLE(K)*(1.0,+R)
S = R*X*(NL,K)

```

```

XLE(K) = XLE(K) - S
DO 52 I=1,N
XS{I,K} = XS{I,K}*{1,+S
52 YS{I,K} = YS{I,K}*(1.+R)
61 K IF (K.L.E.NS) GO TO 11
Z0 (KS)*NE*01 Z0 = ZS(1) *ZS(NS)
1F (KS)*NE*01 Z0 = ZS(1)
DO 62 K=1,NS
XTFO = AMAX1(XTE0,XS(1,K))
ZS(K) = ZS(K)-Z0
62 ZTIP RETURN
      = ZS(NS)
500 FORMAT(1X)
510 FORMAT(1H10.6)
600 FORMAT(1H1)
610 FORMAT(F12.4,7F15.4)
ENC

```

```

C***SUBROUTINE COORD (NX,NY,NZ,KSYM,ZLIM,XLIM,YLIM,ZLIM,
1      SY,AZ,AY,AZ,PX,PZ,AQ,BQ,ZO)
C      SETS UP STRETCHED PARABOLIC AND SPANNING COORDINATES
C      DIMENSION AO(1),BO(1),Z0(1)
PI = 3.1415926535898
BOUND = .95
AX = .5
AY = .5
AZ = .625*BUND
XLIM = .625*BUND
SY = .5
SCALZ = ZLIM/(1.000001*ZLIM)
LX = NX/2+1
DX = NX/2+1
GR = PI/XLIM
PX/C = R*SIN(Q) -XLIM
DO 12 I=1,NX
D = (I-1)*DX
Q = ABS(D)*LE.XLIM GO TO 12
IF (D.LT.0.) B = -1.0
A = 1.0*A*X
C = B*XLIM +(D - B*XLIM)/C
12 AO(I) = D/NY +1
KY = BOUND/NY
DO 22 J=1,KY
D = (KY - J)*DY
A = 1.0*-D*D
C = A**AY
22 BO(J) = SY*D/C
K1 = NZ/2+1
K2 = NZ +1
DZ = 2.0*BUND/NZ
Q = PZ/C
R = (KSYM.EC.O) GO TC 31
IF (KSYM.EC.O) GO TC 31
LZ = NZ +3
K1 = LZ
K2 = NZ/NZ

```

```

31      Q = Q + Q
      R = -PZ/Q
      D = 1.0/K1
      K = K2
      D = (K - LZ)*DZ
      D = D + R*SIN(Q*D)
      IF (ABS(C) > ZLIM) GOTO 32
      B = 1.0/(E*C)
      IF (D < 0.0) B = -1.0
      A = A**AZ
      C = B**ZLIM
      D = C + (D - B*ZLIM)*E)**2
      Z0(K)
      RETURN
END
32

```

```

C** SUBROUTINE SINGL***** SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHORDO,ZS,XLE,YLE,
      SUBROUTINE SINGL (NS,NZ,KSYM,KTE1,KTE2,FUS,CHORDO,ZS,XLE,YLE,
      GENERATES SINGULAR LINE FOR SQUARE ROOT TRANSFORMA TION
      DIMENSION ZS(1),XLE(1),YLE(1),XO(1),YC(1),ZD(1),YPO(1),ZPO(1),
      1. K1 = 1
      K2 = NZ +1
      K1 = 2
      K2 = NZ +3
      KTE1 = 3
      11 DO 12 K=K1,K2
      IF ((Z0(K)*LT.ZS(1)),KTE1 = K
      IF ((ZC(K).LE.ZS(NS)),KTE2 = K
      12 CONTINUE
      CALL SPLIF ((1,NS,Z$XLE,E1,E2,E3,Z$0,C0,IND)
      CALL SINPL ((KFE1,KTE2,Z$X0,NS,Z$YLE,E1,E2,E3,0)
      S1 = CHORDO*TAN(SWEEP)
      S2 = CHORDO*EI(NS)
      CALL SPLIF ((1,NS,Z$YLE,E1,E2,E3,Z$C0,IND)
      CALL SINPL ((KFE1,KTE2,Z0YC,NS,Z$YLE,E1,E2,E3,0)
      T1 = CHORDO*EI(NS)
      T2 = CHORDO*EI(NS)
      XO((KTE1-1)) = X0((KTE1)) + X0((KTE1+1))
      YO((KTE1-1)) = YO((KTE1)) + YO((KTE1+1))
      IF (KSYN.NE.0) GO TO 31
      DU 22 K=K1,N
      ZD = (Z0(K))-ZC((KTE1))/CHORDO
      A = EXP(ZD)
      X0(K) = X0((KTE1)) + S*ZD - (S1/-T1)*(I,-A)
      YO(K) = YO((KTE1)) + T*ZD - (T1/-S1)*(I,-A)
      31 DO 32 K=N,K2
      ZD = (Z0(K))-Z0((KTE2))/CHORDO
      A = EXP(-ZD)
      X0(K) = X0((KTE2)) + S*ZD + (S2/-T2)*(I,-A)
      YO(K) = YO((KTE2)) + T*ZD + (T2/-S2)*(I,-A)
      32 DO 42 K=K1,K2
      ZPO(K) = YO(K)
      IF ((FUS.LE.C.) GO TC 42
      A = .25*(ZQ(K)**2 - YO(K)**2)
      B = .5*ZQ(K)*YO(K)
      S = SQRT(A**2 + B**2)

```

```
IF (S.G1.C0.) = 0° T = 5*ATAN2( B,A )
      S = SQR(T)(S)
      YPO(K) = .5*Y0(K) + S*SIN(T)
      ZPO(K) = .5*Z0(K) + S*COS(T)
CONTINUE
RETURN
END
```

42

```

C**SUBROUTINE SURF*****SUBROUTINE SURF (NC,NE,NS,NX,NZ,ISYM,KTE1,KTE2,
1      YAW,XTE0,XL,IN,FX,NP,XS,Y,S,SLCPY,TRAIL,
2      AO,XO,ZO,SO,SCAL,L3,AC)
3      XP,YP,SURFACE,AJ,ME,SH,POINTS
4      SO(NE,1)XS(ND,1),YS(NC,1),ZS(1),SLOPT(1),TRAIL(1),
5      AO(1),XO(1),ZO(1),SCAL(1),L2(1),
6      XP(1),YP(1),SN(1),D1(1),D2(1),D3(1),
7      XIV(LNE,1),NP(1),ITE1(1),ITE2(1),
8      13*1415*26*3589*E
9      PI=TAU(YAW)
10     TYW
11     SS0=XTE0/XLIM**2
12     DX==2*/NX
13     LX==NX/2+1
14     MX==NX+1
15     MZ==NZ+3
16     IV0==1-ISM
17     IV1==1-1-ISM
18     DO2,K=1,NZ
19     ITE1(K)=MX
20     ITE2(K)=MX
21     DO2,I=1,NX
22     IV((I,K))=-2
23     SO(I,K)=0*KTE1
24     K2==K2+1
25     K1==K2-1
26     R2=(ZS(K2))-2*0(K1)+2*25(K1)/23(K2)-2S(K1)
27     R2=(ZS(K1))-2*0(K2)+2*25(K2)/23(K1)-2S(K2)
28     R1=(I3*NX)/16+1
29     NX=NX+2-I2
30     (FIX*EG*C)=R1*X((1,K1))/SQR((C/S/50))+R2*X((1,K2))
31     CC=DO2,I=2,NX
32     IF((AC(1))+5*DX)*LT(CC),11,-1+1
33     IF((AC(1))-5*DX)*LT(CC),12,-1+1
34     CONTINUE
35     KK=RR
36     ANGL=U
37     K1=NP(KK)
38     PI+=P1
39     L=0.

```

```

DO 42 I=1,N
R = SQRT(XS(I,KK)*I*2 + YS(I,KK)*I*2)
IF (R .EQ. C) GO TO 43
ANGL = ANGL + ATAN2((U*YS(I,KK) - V*XS(I,KK))/
                           (U*XS(I,KK) + V*YS(I,KK)))
1 U = XS(I,KK)
   = YS(I,KK)
   = SQR((R + R)
   = R*CCS(.5*ANGL)
   = R*SIN(.5*ANGL)

42 U XP(I) = PI
   YP(I) = -1.
   XP(I) = 0.
   YP(I) = 0.

42 CONTINUE = AO(12)/AMIN1(ABS(XP(1)),ABS(XP(N)))
SS = .5/S**2

DO 44 I=1,N
XP(I) = S*XP(I)
YP(I) = S*YP(I)
ANGL1 = ATAN(YS(N,KK)/XS(N,KK))
ANGL2 = ATAN(YS(N,KK)/XS(N,KK))
ANGL1 = ANGL -.5*(ANGL1 - TRAIL(KK))
ANGL2 = ANGL -.5*(ANGL2 + TRAIL(KK))
T1 = TAN(ANGL1)
T2 = TAN(ANGL2)
CALL SPLIF((1,N,XP,YP,D1,D2,D3,I,T2,O,IND)
IF (INC.O) WRITE(6,500) K1,K2,N,FR,R1,R2,ZS(KK)
500 FORMAT(12HOBAC MAPPING,4,10,4,G13:4)
CALL INTPL((1,12,A0,S1,1,N,XP,YP,C1,D2,D3,C)
X1 = SLOPE((1,KK)*(XS(1,KK) - X1))
A = 1/(XS(1,KK) - X1)
BANGL = PI
U = PI
V = 0.
Y = 1.
DO 52 I=2,M
XX = SS*AO(I)*I*2
DX = B*((XX - X1)
Y = YS((1,KK) + A*ALOG(D)/D
R = SQR((X**2 + Y**2)
ANGL = ANGL + ATAN2((U*YY - V*XX), (U*XX + V*YY))
U = XX
V = YY

```

```

52 R SN(I) = S* SCRT(R +R)
      A = SLGFT(K)*XS(N,KK) -X1)
      ANGL = 1. / (XS(N,KK) -X1)
      U V = 0. = 0. +1
      M DO 54 I=N,NX SS*AO(I)**2
      XX = B*(XX -X1)
      D = YS(N,KK) +A*ALOG(D)/D
      YY = SQRT(XX**2+YY**2)
      R = ANGL +ATAN2((U*YY -V*XX), (U*XX +V*YY))
      ANGL = XXX
      U V = YY = S* SCRT(R +R)
      R = R*SIN(.5*ANGL)
      DO 62 I=2,NX
      D2 SO(I,K) = SO(I,K) +RR*SN(I)
      IF (KK.EC.K2) GC TC 71
      KK = K2
      RR TO 41 = R2
      GO TO 41 = SSO
      71 SS (FIX.EQ.0.) = SSO
      1 IF (R1*XS(1,K1) +R2*XS(1,K2)) / (AO(I1)**2 -SO(I1,K1)**2)
      SCAL(K) = SS +SS
      ITIE1(K) = I1
      ITIE2(K) = I2
      ZV(K) = ZO(K) -T YAH*(X0(K) +SS*AC(I1)*AO(I1))
      DO 72 I=11,I2
      IV(I,K) = I2
      M DO 74 I=1,N = I1 -1
      ZZ = ZO(K) -T YAH*(X0(K) +SS*AO(I1)*AO(I1))
      1F (ZZ*EE.ZV(KTE1)) IV(I,K) = IV0
      74 CONINE = I2 +1
      M DO 76 I=N,NX = I2 +1
      ZZ = ZO(K) -T YAH*(X0(K) +SS*AO(I1)*AO(I1))
      1F (ZZ*EE.ZV(KTE1)) IV(I,K) = IV0
      76 CONINE = K2 -1
      K2 = K +1
      1F (K.LE.KTE2) GC TC 21
      K1 = K2
      K2 = NZ

```

```

IF (KSYR.EC.0) GC TC 81
K1 = 3
K2 = NZ +2
81 SCAL(K) = SCAL(KTE2)
DO 82 I=1, MX
Z2 = ZO(K) - T YAW*(XO(K) + SS*A0(I)*A0(I))
IF (Z2.LE.ZS(NS).AND.ZZ.GE.ZV(KTE1)) IV(I,K) = IV0
82 CUNTLE = K +1
IF (K.LE.K2) GO TO 81
SCAL(K) = SCAL(KTE2)
N = KTE2
IF (YAH.LE.0) GO TO 93
I0 = ITE1(KTE2) +1
DO 92 I=I0,LX
N = ZV(N) = ZO(KTE2) - TYAW*(XO(KTE2) - SS*A0(I)*A0(I))
92 I = KTE1
ZV(KTE1-1) = ZO(KTE1-1) - TYAW*(XC(KTE1) + SS*A0(I)*A0(I))
ZV(N+1) = ZO(KTE2+1)
93 DO 102 K=K1,K2
I = 2
IV(I,K) * GT 0! GC TC 104
IF (IV(I+1,K+1) * GT * G. OR. IV(I-1,K+1) * GT * G) IV(I,K) = IV1
IF (IV(I+1,K-1) * GT * G. OR. IV(I-1,K-1) * GT * G) IV(I,K) = IV1
102 CONTINUE
IF (SO(LX,K) .LT. 1.E-05) IV(LX,K) = 0
IF (KSYR.NE.0) RETURN
DO 112 K=1,N
112 SCAL(K) = KTE1 -1
RETURN
END

```

C\*\* SUBROUTINE ESTIM\*\*\*  
SUBROUTINE ESTIM

C INITI AL ESTIMATE OF REDUCED POTENTIAL  
COMMON G(161,18,3),S0(161,35),VORT(115),ZV(115),  
IV(161,35),ITE1(35),ITE2(35),  
AO(161,18),B0(18),X0(35),YC(35),ZC(35),SCAL(35),  
NX,NY,NZ,KTE1,KTE2,ISYM,FUS,MKS,YAW,CYAH,SYAW,ALPHA,CA,SA,FNACH,N1,N2,N3,JC  
MX = NX +1  
NY = NY +2  
NZ = NZ +3  
M2  
DO 12 I=1,161  
DO 12 J=1,1E  
DO 12 K=1,3  
12 G(I,J,K) = 0.  
DO 22 K=1,M2  
WRITE (N3) ((G(I,J,1),I=1,MX),J=1,NY)  
WRITE (N1) ((G(I,J,1),I=1,MX),J=1,NY)  
22 CONTINUE  
K1 = KTE1  
K2 = KTE2  
DO 32 K=K1,K2  
VORT(K) = 0.  
32 RETURN  
END

```

C** SUBROUTINE MIXFLO ****
C      SUBROUTINE MIXFLO FOR MIXED SUBSONIC AND SUPER SONIC FLOW
C      SOLUTION OF EQUATIONS FOR MIXED SUBSONIC AND SUPER SONIC FLOW
C      USING FINITE VOLUME SCHEME
COMMON G(161,183),SO(161,35),ITE1(35),ITE2(35),
     1   IV(161,135),BO(181,35),YC(35),Z0(35),SCAL(35),
     2   AX(161,181),NZ,KTE1,KTE2,ISYM,FUS,
     3   NYAW,ICY,AH,SYAW,ALPHA1,CA,SA,FMACH,N1,N2,N3,I0
     4   COMMON /SPAY/ GL(161,181),QQL(161,181),FL(161,181),
     1   GL(161,181),VLL(161,181),CL(161,181),
     2   AL(161,181),BL(161,181),CL(161,181),
     3   RESL(161,181),
P1,P2,P3,FRES,IRES,KRES,ARES,DG,IG,KG,AG,NSUP
COMMON /FLC/
COPMON/SWPF/
LX=NY,LX,MX,KY,MY,J1,K1,FMACH2,A0,Q1,Q2,RV,TYAW,TOT
NX=+1
KY=NY,+1
MY=NY,+2
J1=2
IF (FMACH .GE. 1.0) J1 = 3
TYAW=SYAW/G,YAW
FMACH2=FMACH**2
A0=1.0/FMACH**2 + .2
C1=2.0/F1
Q2=1.0/F2 -1.0
TOT=0.0
FRES=0.0
ARES=0.0
DG=0.0
AG=0.0
NSUP=0.0
K1=3
K2=NZ+2
IF (KSYM.EQ.0.1) GO TO 1
K1=2
IF (FMACH .GE. 1.0) K1 = 3
K2=NZ
DO 2 M=2,3
READ (N1,ERR=101) ((G(I,J,M),I=1,MX),J=1,MY)
CONTINUE
K=1
NV=KTE1 -1
RV=2.
DO 12 I=1,NY
DO 12 J=1,MX
GL(I,J,1)=G(I,J,2)

```

```

QQ_L(I,J) = 0.
FL(I,J) = 0.
UL(I,J) = 0.
AL(I,J) = 0.
BL(I,J) = 0.
CL_S(I,J) = 0.
REF(K,S,N,E,O) GO TO 21
CALL YSHEEP = 1.
RV TO 51
DO 22 J=1,MY
G(1,J,2) = G(1,J,3)
GL(1,J,2) = G(1,J,3)
22 READ (N1,ERR=101) ((G(1,J,1),G(1,J,3)),J=1,MY)
WRITE (N2) ((G(1,J,1),G(1,J,3)),J=1,MY)
K TO 51
GO TO 51
31 CALL YSHEEP
RV IF (K*NE*KTE2*OR(YAH*LE*0.1 GO TO 51
10 DO 42 I=1,T(K)+1
DO 42 I=10,LX
M V = NX +2 -I
= G(M,KY,1) -G(I,KY,1)
= NV +1 +P3*(V -VORT(NV))
42 VORT(NV) = VORT(NV)
IF (K*EC*K2) GO TO 61
DO 52 J=1,MY
G(1,J,1) = G(1,J,2)
GL(1,J,1) = G(1,J,3)
52 READ (N1,ERR=101) ((G(1,J,1),G(1,J,3)),J=1,MY)
WRITE (N2) ((G(1,J,1),G(1,J,3)),J=1,MY)
K TO 51
GO TO 51
61 DO 62 N=2,3
62 WRITE (N2) ((G(1,J,M),I=1,MX),J=1,MY)
CONTINUE
FRES = FRES/64.*TOT
ARES = ARES/64.*TOT
AG = AG/TOT
10 RETURN = 0
101 10

```

RETURN  
ENC





```

B = *SQRT(A**2+B**2)
S = 0
T = IF (S .GT. 0.) T = 5*ATAN2(B/A)
IF (B .EQ. C .AND. YM(I).GT.(FS + FS)), T = .5*FI
IF (B .EQ. C .AND. YM(I).LT.-(FS + FS)), T = -.5*FI
IF (B .EQ. C .AND. SQR(S) = 0.0) T = -.5*PI
YM(I) = SQR(YM(I)) + S*SIN(T)
ZM(I) = S*ZM(I) + S*COS(T)
A = 2.5*(ZRM(I)**2 - YRM(I)**2) + FS**2
B = 5*ZRM(I)*YRM(I)
E = 0
T = SQR(A**2 + B**2)
S = IF (S .GT. 0.) T = 5*ATAN2(B,A)
YRM(I) = S*YRM(I) + S*SIN(T)
ZRM(I) = 5*ZRM(I) + S*COS(T)
24 DO 32 I=1,N
XX = X(I+1) - XRM(I+1) - XRM(I)
1 XY = X(I+1) + X(I+1) - XM(I+1) - XM(I)
1 XZ = X(I+1) + X(I+1) - XM(I+1) - XM(I)
1 YX = YR(I+1) + YR(I+1) + YRM(I+1) + YRM(I)
1 YY = YR(I+1) - YR(I+1) + YM(I+1) - YM(I)
1 YZ = YR(I+1) + YR(I+1) - YM(I+1) + YM(I)
1 ZX = ZR(I+1) - ZR(I+1) + ZRM(I+1) + ZRM(I)
1 ZY = ZR(I+1) + ZR(I+1) - ZRM(I+1) - ZRM(I)
1 ZZ = ZR(I+1) + ZR(I+1) + ZRM(I+1) + ZRM(I)
1 FX X = YY*ZZ - YZ*ZY - YY*ZZ
F Y X = YY*ZX - ZY*XY - ZY*ZX
F Z X = ZZ*XY - ZY*ZX - ZY*XY
F X Y = ZZ*YY - XY*YY - XY*YY
F Z Y = XX*YY - XY*YY - XY*YY
F X Z = XX*XX - XY*XY - XY*XX
F Z Z = FX*XX + FY*XY + FZ*XZ
FH(I) = 1./FM(I)
A = G(I+1,J,2) - G(I,J,2) + G(I+1,J+1,2) - G(I,J+1,2)
GX =

```



```

UV = QQ(L(I,J)) + U(L(I,J))
BV = (VR + VL(I,J)) * QQR
CV = (WR + WL(I,J)) * FR
UR = WR / AA - 2 * QC
AA = QQ / AA
QA(I) = RE SO(I) / (F * AA)
QP(I) = Q(I)
C(I) = 0.
R(I) = 0. * AMAX1(ABS(U), ABS(V), ABS(W))
FU(I) = F*U * ABS(V)
FV(I) = F*ABS(W)
FW(I) = F*ABS(W)
IF(NSUP(I) . LE. 1 .) G(TC 42
NSUP(I) = NSUP +1
A*(I+1) = A*(I+1) * -1. / QA(I))
FUL(I) = F*U * U
FUV(I) = F*V * V
FWK(I) = F*W * W
GX(X) = G(I+1,J+2) - G(I,J+2) - G(I,J+2)
GY(Y) = G(I,J+1,J+2) - G(I,J+2) + GL(I,J+2)
GZ(Z) = G(I+1,J+1,J+2) - G(I,J+1,J+2)
GXY = G(I+1,J+1,J+2) + G(I,J+1,J+2)
1 GYZ = G(I+1,J+1,J+3) - G(I,J+1,J+3) + GL(I,J+1,J+2)
GZX = G(I+1,J+1,J+3) - G(I,J+1,J+3) - GL(I,J+1,J+2)
FX(X) = F*U * V * GXY
FY(Z) = F*V * W * GYZ
FZX = F*W * U * GZX
P(I) = FUU(I) * GXX + FXY
G(I) = FVV(I) * GYY + FYZ
R(I) = FWV(I) * GZZ + FZX
CONTINUE = FWW(I) * GZZ + FYZ
42 PF P(2) = -P(2)
DO 52 I=2,NX = RESC(I) * RV
AV = PF
PB = PF
PF = P(I)
IF ((FU(I) + F(I+1)) * LT.O.) PF = -P(I+1)
A = UP(I) - UP(I-1) + UM(I) - VM(I-1)
1 + VP(I) + VP(I-1) - VP(I) - VM(I-1)

```



JRES

63 AG =  $\frac{AG}{I}$  + AES(CC(I))  
IF (ABS(CC(I)) \* LE. ABS(DG)) GO TO 62  
DG = CG(I)

JG KG == J K -1

62 DO 72 I=1, Nx = QK(I)  
DO P(I), DP(I), UP(I), WP(I), AP(I), CP(I), ABP(I), CAP(I), ABCP(I)

71 DO 72 I=1, Nx = QK(I)

DP(I), UP(I), WP(I), AP(I), CP(I), ABP(I), CAP(I), ABCP(I)

UP(I), WP(I), AP(I), CP(I), ABP(I), CAP(I), ABCP(I)

WP(I), AP(I), CP(I), ABP(I), CAP(I), ABCP(I)

AP(I), CP(I), ABP(I), CAP(I), ABCP(I)

CP(I), ABP(I), CAP(I), ABCP(I)

ABP(I), CAP(I), ABCP(I)

CAP(I), ABCP(I)

ABC(I), ABCP(I)

72 JF (J - KY) = J21 E2(K) 101  
112 JITE2(K) \* EQ. NX 12 = NX  
11F (ISYK \* EQ. 1) 12 = NX  
DO 82 I=1 NX  
11F (IV(1,K) \* EC \* 1) EQ. 2 \* OR. IV(1+1,K) \* EQ. 2 1 GO TO 83  
1F (IV(1,K) \* EC \* 1) EQ. 2 \* OR. IV(1+1,K) \* EQ. 2 1  
M QK(I) = NX \* 1  
QK(I) = QQP(M)  
DM UW VW AM BM CM ABY(CM)  
UW VW AM BM CM ABY(CM)  
VW AM BM CM ABY(CM)  
AM BM CM ABY(CM)  
BM CM ABY(CM)  
CM ABY(CM)  
ABY(CM)  
CAY(CM)  
ABC(I) E2  
GO TO 82  
QK(I) = QQP(I)  
DM(I)

```

FM(I)
UM(I)
WM(I)
AM(I)
BM(I)
CM(I)
ABN(I)
BCN(I)
CAK(I)
ABCN(I)
CONTINUE
DO 92 I=2,NX
IF (IAE(I,V,I,K)) .GT.1) GO TO 92
RE SD(I) = 0.
A = -A*B(I,I)
S = -B*C(I,I)
1 RESL(I,J)
AL(I,J) = A.
BL(I,J) = 1.
CL(I,J) = 0.
S2 CONTINUE
GO TO 41
101 S1 = 5*SCAL(K)
I1 = NX+2-K
II = ITE(I,K)
N = NV
IF (I.EF.II.OR.ISYM.EQ.1) GO TO 103
YY = G(I2,KY,2)
NV = NV+1
VORT(NV) = VORT(NV) + P3*(V - VORT(NV))
N = NV
I = I - 1
V = 0.
IF (IV(I,K)*NE*1) GC TC 109
ZZ = ZO(K)
NV = NV+1
VORT(NV) = VORT(NV) - P3*(V - VORT(NV))
N = NV
I = I - 1
V = VGR(N)
A = A*(V-A)*VCF(K-1)
105 N = NV+2-K
GO TO 105
107 A = (ZV(N-1)/(ZV(N)-2V(N-1)))
V = NX+2-K
M = G(M,KY-1,2)
G(N,KY-1,2) = G(I,KY-1,2)
G(N,KY-2) = G(I,KY-2)
IF (I.G1=1) GO TO 103
G(I,KY,2) = -G(I,KY,2)

```

```
G(P,KY,2)
G(LX,KY+1,2) = *5*V
RETURN
END
```

```

C***SUBROUTINE VELC*** (K, SV, SM, CP, XP, YP, XMAX, XMIN, YMAX, YMINT)
C
SUBROUTINE VELC (VELCITY, VELFACE, SURFCALC, G, COMMON)
COMMON /SPACER/ IY(161,185), BO(18), X0(35), Y0(35), Z0(35), SCAL(35),
NX(161,18), KTE1, KTE2, ISYM, KSYM, FU(N1,N2, N3, 10),
YA(161,18), SYAW, ALPHA, CA, SA, FACH, N1, N2, N3, 10
COMMON /SPA/ XL(161,18), YL(161,18), ZL(161,18),
XL(161,18), YR(161,18), ZR(161,18),
RESL(161,18), RESU(161,18), WW(161), CP(11), YP(11)
COMMON /UVW/ UV(11), SW(11), XW(11), YW(11)
DIMENSION JCN = 3, 1415, 5265, 389, E
PI = 3.141592653589E
Q1 = 1.2*FMACH**2
T1 = 1.7*FMACH**2
MX = NX + 1
NMAX = 15
AV = 1.0
IF (KSYM.EQ.1 .AND. K.EQ.KTE1) GO TO 1
NMAX = 2
AV = 2.5
1 IF (K.NE.KTE1) GO TO 11
N DO 2 J=1,2
DO 2 I=1,N
X(I,J) = 0.0
Y(I,J) = 0.0
Z(I,J) = 0.0
XR(I,J) = 0.0
YR(I,J) = 0.0
ZR(I,J) = 0.0
N = N + 1
XRS = X0(N)/SCAL(KTE1)
YRS = Y0(N)/SCAL(KTE1)
ZRS = Z0(N)/SCAL(KTE1)
S1 = FS/SCL(KTE1)
DO 12 J=1,2
M = NY + 2 - J
DO 12 I=1,M
XL(I,J) = X(I,J)
YL(I,J) = Y(I,J)
ZL(I,J) = Z(I,J)
XS(I,J) = XR(I,J)

```

$\begin{aligned}
& Y(I,J) \\
& ZR(I,J) \\
& XR(I,J) \\
& YR(I,J) \\
& ZR(I,J) \\
& IF (FS * LE * 0.) \quad GC \quad TC \quad 21 \\
& DO 14 \quad J=1,2 \\
& DO 14 \quad I=1,NX \\
& A = 2.5 * (ZR(I,J)**2 - YR(I,J)**2) \quad +FS**2 \\
& B = 5 * ZR(I,J) * YR(I,J) \\
& S = SQRT(A**2 + B**2) \\
& T = 0 \\
& IF (S * GT * 0.) \quad T = 5 * ATAN2(B,A) \\
& IF (B * EC * 0. AND YR(I,J) * GT * (FS + FS)) \quad T = 5 * PI \\
& IF (B * EC * C * AND T(S) * SQRT(S)) \quad T = -5 * PI \\
& SQR(T(S)) \\
& YR(I,J) = 0.5 * YR(I,J) + S * SIN(T) \\
& ZR(I,J) = 0.5 * ZR(I,J) + S * COS(T) \\
& IF (N * LE . K) \quad GO TO 11 \\
& J = 1 \\
& DO 22 \quad I=2,NX \\
& U = 0. \\
& V = 0. \\
& W = 0. \\
& X = 0. \\
& Y = 0. \\
& Z = 0. \\
& XX = 0. \\
& XY = 0. \\
& XZ = 0. \\
& YY = 0. \\
& YZ = 0. \\
& ZX = 0. \\
& GY = 0. \\
& GX = 0. \\
& GZ = 0. \\
& FX = 0. \\
& FY = 0. \\
& FZ = 0. \\
& F2X = 0. \\
& F2Y = 0. \\
& F2Z = 0. \\
& F = 0. \\
& 1. / (FX * XX + FY * XY + FZ * XZ)
\end{aligned}$

```

U = U + (FXX*GX + FYX*GY + FZX*GZ) * F + CA
V = V + (FYX*GX + FYY*GY + FZY*GZ) * F + SA
W = W + (FXZ*GX + FYZ*GY + FZZ*GZ) * F + SYAW

IF (M.EC.2) GO TO 25
      X = X(1,1) - X(I-1,1)
      Y = Y(1,1) - Y(I-1,1)
      Z = Z(1,1) - Z(I-1,1)
      G = G(I,J,2) - G(I-1,J,2)

GO TO 27
      N = N.EC.NMAX
      GO TO 27

25
      XX = X(1,1) - X(I+1,1)
      XY = X(1,1) - XL(I+1,1)
      YX = Y(1,1) - YL(I+1,1)
      YY = Y(1,1) - YL(I+1,1)
      ZX = Z(1,1) - ZL(I+1,1)
      ZZ = Z(1,1) - ZL(I+1,1)
      GX = G(I,J,2) - G(I,J,1)
      GZ = G(I,J,2) - G(I,J,1)

      GO TO 27
      U = AV*L
      V = AV*V
      W = AV*W

27
      UU(1,1) = L
      VV(1,1) = V
      WW(1,1) = W
      U = U*U + V*V + W*W
      V = SQR(I(Q))
      W = AMAX(SV(1)/SQR(Q))
      I = I1*(Q**3.5**(-1.0))
      K = SCAL(KTE1)**X(I,1)
      L = SCAL(KTE1)**Y(I,1)
      M = SITE1(K)
      N = SITE2(K)
      O = SCAL(KTE1)**X(I1,1)
      P = SCAL(KTE1)**Y(I1,1)
      Q = XMAX
      R = YMAX
      S = XMAX
      T = SCAL(KTE1)*Y(I1,1)
      U = AMAX(XMAX,XP(I,1))
      V = AMIN(XMIN,XP(I,1))
      W = AMAX(YMAX,YP(I,1))
      X = AMIN(YMIN,YP(I,1))

DO 22 I=I1,12
      XMAX = AMAX(XMAX,XP(I,1))
      XMIN = AMIN(XMIN,XP(I,1))
      YMAX = AMAX(YMAX,YP(I,1))
      YMIN = AMIN(YMIN,YP(I,1))

22
      RETURN
END

```

```

***C**SUBROUTINE CPLCT*****
SUBROUTINE CPLCT (13,14,FMACH,XP,YP,CP,SM,11,12,KPLOT)
PLCTS CFA COMPUTATIONAL MESH PCNTS
COMMON /PCKR/ PTCK
COMMON /PARMT3/ XT3(161),YT3(161),ZT3(161)
1 COMMON /UVW/ UU(161),VV(161),WW(161)
COMMON /PRSS/ XQCD(161)
COMMON /SFARE/ LJNE(90),DUMMY(10)
COMMON /KODE/ (2)XP(1),YP(1),CP(1),SM(1)
DATA I$1/1H+/ DATA I$2/1H+/
NOI = C
IMIN = 11 + ((12 - I1)/2
ICH = XF(11) - XP(IMIN)
2 FORMAT(40H0PLOT OF CP AT COMPUTATIONAL MESH POINTS /
1 ICH X 1CH Y 7HMACH NO., 8H CP ,
2 7H XCC *2X 5tCP * 1FB*4*2X 7HC*GRD =.F1C-.4)
CPC = ((1. + 2*FMACH**2)**3.5 - 1.)/(1.7*FMACH**2)
DO 12 I=1,90
12 LINE(1) = KODE(1)
CPS = (((15.+FMACH**2)**6/6.)*3-1.)/(1.7*FMACH**2)
IF (KPLOT.EQ.0.CR.KPLOT.GT.1) GO TO 15
15 WRITE(6,CPS,CHE
CONTINUE
KS = 3C**((CPO - CPS) + 4.5
IF (KS.GE.1.0 AND. KS.LE.90) LINE(KS)=IST
DO 22 I=13,14
22 K = 30.*((CPO - CP(1)) + 4.5
= MIN(9C,K)
LINE(K) = KODE(2)
XOC = (XF(I)-XP(IFIN))/CHD
IF (KPLCT.EQ.0.CR.KPLOT.GT.1) GC TC 20
WRITE(6,61C) XP(I),YP(I),SM(I),CP(I),XCC,LINE
CONTINUE
LINE(K) = KODE(1)
IF ((I.LT.11.OR.I.GT.12) GO TO 22
NOI = ACI + 1
XT3(NOI) = XP(I)
YT3(NOI) = YP(I)
ZT3(NOI) = Z
UT3(NOI) = LU(I)
VT3(NOI) = LV(I)
WT3(NOI) = LW(I)
20 IF ((K.EC.KS) LINE(KS)=IST
IF ((KPLCT.EC.0.CR.KPLOT.GT.1) GO TO 25
CALL INVALI
22 IF ((KPLCT.EC.0.CR.KPLOT.GT.1) GO TO 25

```

25 CONTINUE  
61C RETURN (2F10.4, F7.4, F8.4, F7.4, 9CA1)  
ENC

```

C** SUBROUTINE INVRT6 *****
      SUBROUTINE INVR16
      COMMON /PCKR/ PTCK
      COMMON /PARMT3/ XT3(161), YT3(161), ZT3(161),
     1 DIPENSIGN P(161,6), TEMP(161)
      EQUIVALENCE (XT3(1),YT3(1),ZT3(1))
      DO 10 I=1,6
      DO 30 J=1,6
      M=N0I-I+J
      TEMP(M)=F(I,J)
 10 C CONTINUE
      DO 20 I=1,NCI
      P(I,J)=TEMP(I)
 20 C CONTINUE
 30 C CONTINUE
      WRITE(C,100), (1,X)T3(I), ZT3(I), YT3(I),
     1 WT3(I), VT3(I), N0I
      RETURN
 10C FORMAT(4HO 1 ,1X,6HXT3(1),4X,6HZT3(1),4X,6HYT3(1),4X,6HT3(1),
     1   2   6X,4H 1 ,1X,6HXT3(1),4X,6HZT3(1),4X,6HYT3(1),4X,6HT3(1),
     3   4   (14,1X,6E10.3,2X,14,1X,6E10.3)
     4 END

```

```

C***SUBROUTINE FCRCF *****
C   SUBROUTINE FORCF (I1,I2,XP,YP,CP,AL,CHCRD,XM,YM,CL,CD,CM)
C   CALCULATES SECTION FORCE EFFICIENTS
C   DIMENSION IXP(1),YP(1),CP(1),
C   RAD = 57.295779513082
C   ALPHA = AL/RAD
C   CL = 0.
C   CD = 0.
C   CM = 0.
C   DD = 12  I=11  N = 12 -1
C   DX = ((XP(I+1)) - XP(I))/CHORD
C   DY = ((YP(I+1)) - YP(I))/CHORD
C   XA = 1.5*(XF(I+1) + XP(I)) - XM)/CHORD
C   YA = 1.5*(YF(I+1) + YP(I)) - YM)/CHORD
C   CPA = .5*(CP(I+1) + CP(I))
C   DCL = CPA*DX
C   ECE = CPA*DY
C   CL = CL + DCL
C   CD = CD + DCL
C   CM = CM + DCD*YA - DCL*X
C   12  CL = CL*COS(ALPHA) - CD*SIN(ALPHA)
C   CD = CL*SIN(ALPHA) + CD*COS(ALPHA)
C   CL = DCL
C   RETURN
C   END

```

```

C***SUBROUTINE TCTFOR *****
      SUBROUTINE TCTFOR (KTE1,KTE2,CHORD,SCL,SCD,SCM,X0,YPO,ZPO,
     1   C   CALCULATES TOTAL FORCE COEFFICIENTS
     2   DIMENSION SCL(1),SCD(1),SCM(1),X0(1),YPO(1),ZPO(1)
     3   SPAN = ZPO(KTE1)-ZPO(KTE2)
     4
     5   CL  = 0.
     6   CD  = 0.
     7   CMP = 0.
     8   CMR = 0.
     9   CMY = 0.
    10  S   = 0.
    11  KTE1 = KTE1*KTE2*CHORD(K)*CHORD(K)*CHORD(K)*CHORD(K)
    12  QM  = SCD(K)*CHORD(K)*CHORD(K)*CHORD(K)*CHORD(K)
    13  CL  = -5*(ZPO(K+1)-ZPO(K))
    14  CD  = 5*(ZPO(K+1)+ZPO(K))
    15  CMP = SCD(K+1)*CHORD(K+1)
    16  CMR = SCD(K+1)*CHORD(K+1)
    17  CMY = SCD(K+1)*CHORD(K+1)
    18  S   = SCD(K+1)*X0(K+1)*YPO(K+1)+SCD(K+1)*YPO(K+1)
    19  K   = DZ*(PL+CL)
    20  CL  = DZ*(PD+QD)
    21  CD  = CL+CLA
    22  CMP = CD+CDA
    23  CMR = CMR+DZ*(PK+QM)
    24  CMY = CMY+A2*CLA
    25  S   = S+DZ*(CHORD(K+1)+CHORD(K))
    26  PL  = PD
    27  QD  = PM
    28  K   = K+1
    29  IF  ((K.LT.KTE2)) GOTO 11
    30  CL  = CD/S
    31  CD  = CMP*SPAN/S**2
    32  CMR = (CMR+CMR)/(CMY+CMY)/(SPAN)
    33  CMY = RETURN
    34  END

```

```

C** SUBROUTINE REFIN
SUBROUTINE REFIN
HALVES PESH SIZE
COMMON G(1:61,1:18,3) I(0(1:161,1:35),TE(1:161,1:35),
1 G(1:161,1:35),TE(1:161,1:35),VORT(115),ZV(115),
2 A(1:161,1:18),B(1:18,1:35),Y(1:18,1:35),Z(1:18,1:35),
3 NX,NY,NZ,KTE1,KTE2,ISYM,KSYM,FU,S,SCAL(35),
4 YAW,CYAW,SYAW,ALPHA,CA,SA,FNACH,N1,N2,N3,I0
      NX = NY +1
      KY = NY +1
      KZ = NZ /2 +3
      MX0 = NX /2 +2
      MY0 = NY /2 +1
      MZ0 = NZ /2 +1
      K = 1
      IF (KSYM.EQ.0) GO TO 11
      MZ0 = NZ /2 +3
      REAC (N1,ERR=401) ((G(I,J,1),I=1,MX0),J=1,MY0)
      K = 2
      REAC (N1,ERR=401) ((G(I,J,1),I=1,MX0),J=1,MY0)
      J = 1
      J = NY /2 +1
      KY = NY /2 +1
      K = MX0
      I = 1
      G(I,I,JJ,1) = G(I,J,1)
      J = 1
      J = I+1
      I = 1
      IF (I.GT.0) GO TO 31
      J = J-1
      J = J+1
      DO 42 J = 1,2,NX,2
      DO 42 J = 1,2,NX,2
      G(I,J,1) = 0.5*(G(I+1,J,1)+G(I-1,J,1))
      DO 54 J = 1,2,NY,2
      G(I,J,1) = 0.5*(G(I,J+1,1)+G(I,J-1,1))
      G(I,NY,1) = 0.
      WRITE (N2) ((G(I,J,1),I=1,MX),J=1,MY)
      K = K+1
      IF (K.LE.MZC) GC TC 11
      REWIND N2
      READ (N2,ERR=401) ((G(I,J,1),I=1,MX),J=1,MY)
      READ (N2,ERR=401) ((G(I,J,3),I=1,MX),J=1,MY)

```

```

WRITE (N1) ((G(I,J,1), I=1,NX), J=1,NY)
K = 1
IF (KSYR.NE.0) K = 2
111 K = 1
DO 112 I = 1, NY
DO 112 J = 1, NX
DO 112 I = 1, 3 * (G(I,J,1) + G(I,J,3))
112 WRITE (N1) ((G(I,J,1), I=1,NX), J=1,NY)
122 CONJNUF
IF (K.EC.MZC) GC TC 201
DO 132 I = 1, NY
DO 132 J = 1, NX
132 REAC((N2,1,1) = G(I,J,3)
GO TO 201
RE WIND
1 RE WIND A2
DO 202 R = 1, 3
READ (N1,ERR=401) ((G(I,J,3), I=1,NX), J=1,NY)
202 CONTINUE
WRITE (N2) ((G(I,J,1), I=1,NX), J=1,NY)
TYAW = SYAh/CYAW
NV = KTE1 - 1
VORT(NV) = 0.
K = 2
IF (KSYR.NE.0) GO TC 251
S1 = NV
211 N = NV
IF (K.LT.KTE1.OR.K.GT.KTE2) GO TO 231
I1 = NV
I1 = MX0 + 1
I1 = ITE1(K)
I2 = ITE2(K)
DO 212 I = 1, 12
G(I,KY+1,2) = G(I,KY,2) + G(I,KY,2) - G(I,KY-1,2)
NV = NV + 1
VORT(NV) = G(I2,KY,2) - G(I1,KY,2)
N = NV
I = I1
IF (K.NE.KTE2.OR.YAW.LE.0.) GO TO 231
221 M = NV
M = NX + 2 - 1
NV = NV + 1
VORT(NV) = G(M,KY,2) - G(I,KY,2)
IF (I.LT.MX0) GC TD 221
I = I - 1
231 V = 0.

```

```

IF (IV(I,K)*NE.1) GO TO 237
22 IF (ZL*EE.*ZV(N-1)) GO TO 235
N = N - 1
233 GO TO 233 = A*VCRT(N)/((1.-A)*VCFT(N-1))
235 A V = A*VCRT(N)/((1.-A)*VCFT(N-1))
237 M G(I,KY+1,2) = NX +2 -1 = G(M,KY-1,2) -V
G(I,KY+1,2) = G(I,KY-1,2) +V
G(I,KY,(I,K)) = NE * 5*G(I,KY,1) GO TO 241 +G(M,KY,3)
IF (I,KY,(I,K+1)) .LT. 1 .EQ. 5*G(I,KY,3) +G(M,KY,1)
16(I,KY,2) = G(I,KY,2) + 25*(G(I,KY,1)
G(I,KY-1,2) = .5*(G(I,KY,2) +G(M,KY-2,2)
G(I,KY-1,2) = .5*(G(M,KY,2) +G(M,KY-2,2))
241 IF (I*G1*1) GO TO 231
G(I,KY,2) = .5*V
251 IF (K*EG.MZ) GO TO 261
DO 252 I=1,MY K +1
G(I,J,1) = G(I,J,2)
DO 252 I=1,MY K +1,MY
252 WRITE (N2,ERR=401) ((G(I,J,I=1,MX),J=1,MY),I=1,MX),J=1,MY
READ (N1,ERR=401) ((G(I,J,J=1,MY),I=1,MX),J=1,MY)
GO RTN N1 = 0.
261 DO 262 I=1,MY ((G(I,J,M),I=1,MX),J=1,MY)
WRITE (N2,((G(I,J,M),I=1,MX),J=1,MY)
262 CONTINUE
REWIND N1
REWIND N2
DO 302 K=1,MZ
REAC(N2,ERR=401) ((G(I,J,I=1,MX),I=1,MX),J=1,MY)
302 WRITE (N1,ERR=401) ((G(I,J,I=1,MX),J=1,MY)
CONTINUE = 1
RETURN
401 RETURN
ENC

```

```

C**SUBROUTINE SMCC**SUBROUTINE SMOC
      SUBROUTINES FACTENT AL
      COMMON /161/ 18,3,1,SO(161,35),VORT(115),ZV(115),
      /161/ 35,1,ITE1(35),ITE2(35),
      /161/ 18,1,B0(18),X0(35),YC(35),ZO(35),SCAL(35),
      /161/ 18,1,XN2,KTE1,KTE2,ISYM,FUS,
      /161/ 18,1,YAW,CYAH,SYAW,ALPHA,CA,SA,FRACH,N1,N2,N3,I0
      /161/ 18,1,NX,KY,MY,MZ,K1,K2,IF((KSYP*EC*0)) GO TO 1
      K1=NX+2
      K2=NZ+2
      IF(K1=K2) GO TO 1
      1 PX=1./E*
      PY=1./E*
      PZ=1./E.
      DO 2 L=1,3
      READ(N1,ERR=51) ((G(I,J,L)),I=1,MX),J=1,MY)
      2 COUNTINUE
      WRITE(N2) ((G(I,J,1)),I=1,MX),J=1,MY)
      K=K+1
      11 DO 12 I=3,NX
      14 G(1,J,1)=(1.5*PX*(G(I+1,J,2)-PZ)*G(I,J,2)
      14 G(1,J,1)+0.5*PY*(G(I,J+1,2)+G(I,J,2))
      14 G(1,J,1)+0.5*PZ*(G(I,J,3)+G(I,J,1)))
      12 G(MX,J,1)=G(MX,J,2)
      DO 16 J=1,NX
      G(1,1,1)=G(1,1,2)
      G(1,1,2)=G(1,1,3)
      G(1,1,KY,1)=G(1,1,KY,2)
      G(1,1,MY,1)=G(1,1,MY,2)
      16 WRITE(N2) ((G(I,J,1)),I=1,MX),J=1,MY)
      IF((K*EC*K2)) GO TO 31
      DO 22 J=1,NX
      DO 22 I=1,NX
      G(1,J,1)=G(1,J,2)
      G(1,J,2)=G(1,J,3)
      22 READ(N1,ERR=51) ((G(I,J,3)),I=1,MX),J=I,MY)
      GO TO 31
      WRITE(N2) ((G(I,J,3)),I=1,MX),J=1,MY)

```

```
REWIND N1
REWIND N2
DO 42 K=1,MZ
READ (N2,ERR=51), ((G(I,J,1), I=1,MX), J=1,MY)
WRITE (N1) ((G(I,J,1), I=1,MX), J=1,MY)
CONTINUE
42 IO RETURN = 1
51 IO RETURN = 0
END
```

```

C** SUBROUTINE SPLIF(*,*SPLIF(H,N,S,F,FP,FPP,KM,VM,KN,VN,MODE,FQM,IND)
C SPLINEFIT - JAPES C IN FPPP IF MODE GREATER THAN 0
C INTEGRAL PLACED IN FPPP IF CAIA IS LEGAL
C INDSEITC ZERO IF CAIA IS LEGAL
C DINESIGN = 0 IF (1), FP(1), FPP(1) , FPPP(1)
C DINC = 1 IF (K - 1) = IA B S(N - K)
C           = (N - M)/K
1   K   = H
     = N + K
     = DS(J) - S(I)
     = DS
D   DS (DS) 11: 81 F 11
11  DF (KM -2) = {F(J) - F(I)) / DS
12  U   V   TO 25 = 5. * (DF - VM) / DS
     GO TO 25 = 0
13  U   V   TO 25 = VM
14  U   V   TO 25 = -1 * S * VM
     GO TO 25
21  J   .       = J + K
     = S(J) - S(I)
     = DS(D*L*) 81 F 23
22  DF B       = {F(J) - F(I)) / DS
     = 1. / (DS + DS + U)
     = B * DS
     = B * (C.*DF - V)
25  FP(I), U   = V(2 - U)*DS
     = 6.*CF + DS*V
     = 21 31 21
31  IF (KN -2) = 32 33 34
     GO TO 25 = (6.*VN - V)/U
32  V   GO TO 25 = VN
33  V   GO TO 25 = DS*VN + FPP(I)/(1. + FP(I))
34  V   B       = V
     = DS(J) - S(I)
41  DS

```

```

      U FPPP(I)   = FPP(I) - FF(I)*V
      FPF(I)    = (V-U)/DS
      FP(I)     = U(F(J) - F(I))/DS - DS*(V + L + U)/6.
      V         = U

      J IF (J - N) = I - K
      I   = 41, 51, 41
      N   = -K
      FPP(N)  = FPP(I)
      FPP(N)  = B
      FP(N)   = DF + D*(FPP(I)) + B + B)/6.
      INC     = 1
      IF (M0FE)  = 81, 81, 61
      FP FP(J) = FQM
      V     = FP(J)
      J DS   = S(J) - S(I)
      I   = J + K
      DS   = FPP(J)
      FPPP(J) = FPP(I) + .5*DS*(F(I)) + F(J) - DS*DS*(U + V)/12.)
      V IF (J-N) = 71, 81, 71
      I   = 1 INC, EC, 1) INC, MCDE, 1, J^K, M^4/
      F WRITE (6H0CHECK, 10, 4G13.4/
      E WRITE (6E, (S(I), F(I), I=M, N)
      86 FORMAT (10G13.4)
      SC RETURN
      END

```

```

C**SUBROUTINE INTPL*****SI(N,FI,K,N,S,F,FPF,FPPP,MODE)
C      SUBROUTINE INTFL(N,FI,K,N,S,F,FPF,FPPP,MODE)
C      INTERPOLATION USING TAYLOR SERIES - JAPESCN
C      ADCTS CCRECATION FOR PIECEWISE CONSTANT FOURTH DERIVATIVE
C      IF MODE GREATER THAN O
C      DIMENSION S(1),FI(1),S(1),FI(1),FP(1),FPPP(1)
C      K = SAB(N,-M)/K
C      K = M
C      MIN = M
C      D = S(N) - S(M)
C      IF (D*(S(N)) - SI(M))) 11,13,13
11   MIN = M
12   KI = IABS(NIN-MIN)
13   IF (KI) 21,21,E
14   KI = (NIN-MIN)/KI
21   C = 0
22   IF (MODE) 31,31,23
23   C = 1
24   SS = SI(1)
32   IF (I-N) 35,37,35
35   IF (D*(S(I)) - SS) 33,33,37
37   I = 1
38   SS = S(I)
39   FP PPP = FPPP(I)
40   FF = FPP(I)
41   FI (I) = F(I)
42   IF (I) -NIN 31,41,31
43   RETURN
44   ENC

```

```

C** SUBROUTINE VERTEC *****
C   SUBROUTINE VERTEC (11,12,XCCD,CP,NRD,ZPC,FMACH,YA,AL,
1      SCL,SCD,SCM,K)
C
C   SUBROUTINE FOR VERSATEC PLOTTING OF THE PRESSURE COEFFICIENT
C   VS NON-DIMENSIONAL CHORD (X/C) FOR EACH SECTION OF THE FINAL
C   MESH
C
C   REAL PXC(165), PCP(165), XCL0(85), XCLP(85), CPUP(85), CPUD(85),
1      XCCD(161), CP(161), ZPO(35), SCL(35), SCD(35), SCM(35),
2      FMACH, YA, AL
C
C   INTEGER I,J,NUM1,NUM2,NUM3,II,12,NRD,K
C
C   INITIALIZE ARRAYS AND DATA TO ZERO.
C
      NUM1 = C.0
      NUM2 = C.0
      NUM3 = C.0
      DO 10 I=1,165
         PXC(I) = 0.0
         PCP(I) = 0.0
10     CONTINUE
      DO 20 J=1,85
         XCLC(J) = 0.0
         CPLC(J) = 0.0
         XCUP(J) = 0.0
         CPUP(J) = 0.0
20     CONTINUE
C
C   READ IN X/C AND CP DATA INTO NEW ARRAY STARTING AT ARRAY
C   ELEMENT NUMBER 1
      DO 30 I=1,12
         PXC(I+1) = XCCD(I)
         PCP(I+1) = CP(I)
30     CONTINUE
      PXC(NRD) = 1.0
C
C   PUT THE DATA INTO TWO ARRAYS: ONE FOR THE LOWER SURFACE
C   AND ONE FOR THE UPPER SURFACE
      NUM1 = (NRD-1)/2
      NUM2 = NRD+1
      DO 40 I=1,NUM1
         XCLC(I) = PXC(I)
         CPLC(I) = PCP(I)
40     CONTINUE
      DO 50 J=NUM1,NRD
         XCUP(J-NUM1) = PXC(J)
         CPUP(J-NUM1) = PCP(J)
50     CONTINUE
C
C   INITIALIZE THE VERSATEC PLTTER SYSTEM

```

```

C CALL PLTIS (0.0,0.0,0.0)
C SCALE THE DATA TO AN 5.0 X 7.0 INCH SPACE
C CALL SCALE (PXC,5.0,NRD,+1)
C CALL SCALE (PCP,7.0,NRD,-1)

C DRAW THE X AND Y AXES
C CALL AXIS (1.0,2.0,'X/C' ,-3.5,0.0,C*PXC(NRD+1),PXC(NRD+2))
C CALL AXIS (1.0,2.0,'PRESSURE COEFFICIENT (CF)' ,25,
C >7.0,C*PCP(NRD+1),PCP(NRD+2))
C PUT SCALE FACTORS INTO TWO ARRAYS FOR UPPER AND LOWER SURFACE
C XCLC(NR1+1) = PXC(NRD+1)
C XCLC(NR1+2) = PXC(NRD+2)
C CPLC(NR1+1) = PCP(NRD+1)
C CPLC(NR1+2) = PCP(NRD+2)

C XCLP(NR1+1) = PXC(NRD+1)
C XCLP(NR1+2) = PXC(NRD+2)
C CPLP(NR1+1) = PCP(NRD+1)
C CPLP(NR1+2) = PCP(NRD+2)

C PLCT THE DATA POINTS
C CALL NEOPEN (2)
C CALL PLCT (1.0,2.0,'-3')
C CALL LINE ('XCLP',CP1,NUM1,1,-1,11)
C CALL LINE ('XCLP',CP1,NUM1,1,-1,11)

C PLACE TITLE AT TOP OF PAGE
C CALL SYNPEN (3)
C CALL SYNPEN (1,25,7.5,0.2,'SECTION CP DATA ',0.0,1.6)
C CALL SYNPOL (1,25,7.0,0.1,!+* = UPPER SURFACE ',0.0,1.8)
C CALL SYNPOL (1,25,7.0,0.1,!+ = LOWER SURFACE ',0.0,1.8)

C PLACE FCTN INFORMATION ON PLOT
C CALL NEOPEN (2)
C CALL SYNPOL (0.0,-75,C1,'SPAN STATION = ',0.0,1.5)
C CALL SUPPER (9.99,-9.99,0.1,ZPO(K),C0,E)
C CALL SUPPER (9.99,-1.0,0.1,MACF,C0,E)
C CALL SUPPER (9.99,-9.99,0.1,FMACH,C0,E)
C CALL SUPPER (2.0,-1.0,0.1,YAW,C0,E)
C CALL SUPPER (9.99,-9.99,0.1,YA,A0,0,3)
C CALL SUPPER (9.99,-1.0,0.1,ADA,0,0,5)
C CALL SUPPER (9.99,-9.99,0.1,AL,0,0,3)
C CALL SUPPER (0.0,-1.25,0.1,CL,0,0,6)
C CALL SUPPER (9.99,-9.99,0.1,SCL (K),C0,E)
C CALL SUPPER (2.0,-1.25,0.1,CD (K),C0,E)

```

```

CALL NUMBER (995., 999., 0., 1., SCD (K), C, 0., + 5)
CALL SYMCL (4, 0., -1, 25., 0., 1., SCW (K), C, 0., + 5)
CALL NUMBER (995., 999., 0., 1., SCM (K), C, 0., + 5)

C END
      CALL PLCT (0, 0, C, 0, + 995)
      RETURN
      END

```

APPENDIX F

THIS APPENDIX PRESENTS THE SOURCE CODE FOR THE INTERACTIVE PROGRAM FINDIN

C\*\*\*\*\*SYMMETRICAL WING SECTION DATA\*\*\*\*\*  
 DATA SYFFN/59/ 0 / SYNUM/59/ 0 /  
 1 SYMXF/1.05500 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 .  
 2 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 .  
 3 07500 . 07500 . 07500 . 07500 . 07500 . 07500 . 07500 . 07500 . 07500 . 07500 .  
 4 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 .  
 5 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 . 00250 .  
 6 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 .  
 7 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 . 05000 .  
 SYMF/ 0450 . 0475 . 0505 . 0525 . 0550 . 0550 . 0550 . 0550 . 0550 . 0550 .  
 0480 . 0447 . 0398 . 0330 . 0265 . 0265 . 0236 . 0200 . 0167 . 0140 .  
 0090 . 0065 . 0030 . 0063 . 0063 . 0063 . 0063 . 0063 . 0063 . 0063 .  
 - 00230 . - 00265 . - 0030 . - 0036 . - 0039 . - 0044 . - 0140 . - 0167 . - 0200 .  
 - 00550 . - 00555 . - 00530 . - 00525 . - 00525 . - 00505 . - 00480 . - 00560 . - 00540 .  
 - 0375 . - 0340 . - 0290 . - 0240 . - 0240 . - 0180 . - 0130 . - 0075 . - 0025 /  
 C\*\*\*\*\*NAC A 24-30-0 SECTION DATA\*\*\*\*\*  
 DATA N512FN/41/ 0 / N512NUM/41/ 0 /  
 1 N572XF/1.0000 . 0900 . 0800 . 0700 . 0600 . 0500 . 0400 . 0300 . 0200 . 0100 .  
 2 0200 . 0200 . 0200 . 0200 . 0200 . 0200 . 0200 . 0200 . 0200 . 0200 .  
 3 00500 . 01000 . 01500 . 02000 . 02500 . 03000 . 03000 . 04000 . 05000 . 06000 .  
 4 07000 . 08000 . 09000 . 09500 . 09500 . 09500 . 09500 . 09500 . 09500 . 09500 .  
 5 0013 . 0120 . 0204 . 0376 . 0515 . 0642 . 0730 . 0780 . 0780 . 0788 .  
 6 00768 . 007261 . 00661 . 00563 . 00414 . 00356 . 00290 . 00220 . 00168 . 00128 .  
 7 0070 . 00502 . 00302 . 00315 . 00420 . 00422 . 0120 . 0168 . 0227 . 0227 .  
 8 00268 . 00320 . 00260 . 00215 . 00150 . 00082 . 00048 . 00013 . 00013 .  
 C\*\*\*\*\*FLAT PLATE DATA\*\*\*\*\*  
 DATA FPPN/31.0 / FPNLM/31/ 0 /  
 1 FPXP/1.0000 . 0500 . 0300 . 0250 . 0200 . 0150 . 0100 . 0075 . 0050 .  
 2 0025 . 0020 . 0015 . 0010 . 0005 . 0005 . 0005 . 0005 . 0005 .  
 3 0010 . 0015 . 0020 . 0025 . 0030 . 0030 . 0030 . 0030 . 0030 .  
 4 00250 . 00300 . 00300 . 00300 . 00300 . 00300 . 00300 . 00300 . 00300 .  
 FPYF/ 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 .  
 1 0000155 . 0000160 . 0000165 . 0000170 . 0000175 . 0000180 . 0000185 . 0000190 . 0000195 .  
 2 0000045 . 00000425 . 00000400 . 00000375 . 00000350 . 00000325 . 00000300 . 00000275 . 00000250 .  
 3 0000085 . 00000821 . 00000806 . 00000782 . 00000758 . 00000735 . 00000710 . 00000685 . 00000660 .  
 4 0000021 . 00000256 . 00000282 . 00000294 . 00000292 . 00000282 . 00000270 . 00000255 . 00000235 .  
 5 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 .  
 6 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 . 000003 .  
 C\*\*\*\*\*F-14 WING SECTION - TYPICAL\*\*\*\*\*  
 DATA F14FN/47/ 0 / F14NUM/47/ 0 /  
 1 F14XF/1.0590 . 0857 . 0771 . 06571 . 05471 . 04857 . 0286 . 0229 . 0171 . 0114 .

345      0057, -0029, -0057, -0029, -0014, -0020, -0016, -0005, -0006, -0005, -0010, -0020,  
 345      0000, -0000, -0000, -0000, -0000, -0000, -0000, -0000, -0000, -0000, -0000, -0000, -0000,  
 F14YF/ 0000, -0166, -0320, -0451, -0549, -0571, -0574, -0574, -0573,  
 142345      0144, -0457, -0343, -0280, -0185, -0171, -0143, -0114,  
 00076, -0046, -0036, -0023, -0015, -0008, -0007, -0001, -0000,  
 00028, -0037, -0059, -0091, -0115, -0137, -0137, -0160, -0202,  
 00240, -0289, -0343, -0366, -0375, -0375, -0366, -0343,  
 0301, -0229, -0142, -0059, -0000,

C\*\*\*\*\*A7FN/33.0/A7NUM/33/ A7 WING SECTION - TYPICAL\*\*\*\*\*  
 1 A7XF/1.0000, -8000, -6000, -4300, -3000, -2000, -1000, -0750, -0500,  
 2 0250, -0125, -0075, -0050, -0025, -0015, -0010,  
 3 0015, -0025, -0050, -0075, -0125, -0250, -0500, -0750, -1000,  
 4 02000, -03000, -04300, -06000, -08000, -10000, -12000, -14000, -16000,  
 A7YF/ 0000, -01638, -03018, -05017, -07015, -09013, -01102, -01301, -01500,  
 142345      00311, -01610, -02410, -04146, -06170, -08175, -09090, -01321,  
 -00219, -02456, -02659, -02770, -02934, -03130,  
 -03137, -03291, -03373, -03390, -03350, -02897, -03309,  
 -03500, -03018, -01638, -00000,

C\*\*\*\*\*DATA LISFN/49.0/LISNUM/49/ LIS SAMAN 7769 AIRFOIL SECTION\*\*\*\*\*  
 1 LISXF/1.0000, -9500, -9000, -8000, -7000, -6000, -5000, -4000, -3000,  
 2 02009, -01500, -01000, -00750, -00500, -00250, -00125, -00075, -0010,  
 3 0075, -0050, -0025, -00150, -00050, -00025, -000125, -000075, -0010,  
 4 0020, -00100, -00050, -00025, -000125, -000075, -000050, -000025, -0000125,  
 5 00750, -01000, -01500, -02000, -02500, -03000, -04000, -05000, -06000, -07000,  
 LISYF/ 0000, -0041, -0084, -0181, -0216, -0486, -0696, -0897, -0925,  
 142345      00926, -0840, -0706, -0615, -0496, -0406, -0334, -0272, -0245,  
 0171, -0140, -0102, -0094, -0070, -0055, -0051, -0031, -0048,  
 0070, -0080, -0124, -0137, -0164, -0182, -0201, -0216,  
 0230, -00230, -00216, -00170, -0138, -0106, -0091, -0075,  
 0060, -0060, -0045, -0030, -0016, -0008, -0000,

C\*\*\*\*\*DATA N1CFN/37.0/N1CNUN/37/ AIRFOIL SECTION\*\*\*\*\*  
 1 N10XP/1.0000, -5500, -9000, -8000, -7000, -6000, -5000, -4000, -3000,  
 2 02500, -02000, -01500, -01000, -00750, -00500, -00250, -00125, -0050,  
 3 0000, -0050, -0125, -0250, -0500, -0750, -1000, -1500, -2000,  
 4 02500, -03000, -04000, -05000, -06000, -07000, -08000, -09000, -09500,  
 5 0000, -0005, -004952, -00782, -004455, -00985, -01578, -02178,  
 1423      000105, -005092, -01672, -021207, -021137, -03803, -03500, -04412, -04857,



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N63AYF / 7500 • 8000 • 8500 • 9000 • 9500 • 1000 / • 02545 • 02545 • 03044 • 03517 •  
 00021 • 00525 • 01030 • 01535 • 02040 • 02545 • 03044 • 03517 •  
 03943 • 04311 • 04613 • 04837 • 04968 • 04995 • 04913 • 04714 •  
 04400 • 03950 • 03324 • 02917 • 02412 • 01737 • 01250 • 00983 •  
 00815 • 00300 • 00815 • 00833 • 00983 • 01260 • 01412 • 0141295 •  
 -02917 • 03324 • 03950 • 04400 • 04714 • 04913 • 04995 • 04995 •  
 -04968 • 04837 • 04613 • 04311 • 02943 • 03044 • 035044 • 03044 •  
 -02545 • 02040 • 01535 • 01030 • 006525 • 00021 /

```
C-- FILE DEFINITIONS
C-- CALL FRICMS ('FILECEF ','5      ') TERM   ''
C-- CALL FRICMS ('FILEDEF ','8      ') DISK    ''
C-- CALL FRICMS ('CATAIN ','A      ') A
1
```

C-- TITLE PAGE AND INSTRUCTIONS

```

CALL FRICMS ('CLRSCRN ')
WRITE (6,410)
WRITE (6,410)
WRITE (6,420)
WRITE (6,430)
WRITE (6,410)
WRITE (6,410)
WRITE (6,440)
WRITE (6,410)

C-- FIRST LINE INPUT DATA--DEFINE COMPUTATIONAL GRID
C-- CONTINUE
      WRITE (6,450)
      WRITE (6,460)
      READ (5,1000) TITLE
      10   CONTINUE (6,470)
      READ (5,*)
      WRITE (6,480)
      READ (5,*)
      WRITE (6,490)
      READ (5,*)
      WRITE (6,500)
      CALL FRICMS ('CLRSCRN ')
      WRITE (6,500)
      READ (5,*)
      WRITE (6,510)
      READ (5,*)
      FPLOT

C-- SUMMARY OF FIRST LINE INPUT DATA
C-- CONTINUE
      CALL FRICMS ('CLRSCRN ')
      WRITE (6,520)
      READ (5,*)
      IF (ANS .GE. 2) GO TO 20
      WRITE (6,521)
      WRITE (6,522)
      WRITE (6,530)
      READ (5,*)
      IF (ANS .EQ. 1) GO TO 10
      20   CONTINUE

C-- SECCND, THIRD AND FORTH LINES INPUT DATA--ITERATION AND CONVERGENCE
C-- TOLERANCE FOR GRID. NUMBER OF LINES ECALL 10 M = FMESH
      M = IFIX(FMESH)
      CALL FRICMS ('CLRSCRN ')

```

```

      WRITE (6,450)
      DO 30 I=1,N
        IF (I .EQ. 1) WRITE (6,541)
        IF (I .EQ. 2) WRITE (6,542)
        IF (I .EQ. 3) WRITE (6,543)
        WRITE (5,*)
        WRITE (5,550) FIT(I)
        READ (5,*)
        WRITE (5,560) CVO(I)
        WRITE (5,570) COV(I)
        READ (5,*)
        P10(I)
        CALL FRICMS ('CLRSQRN ')
30    CONTINUE

C----- SUMMARY OF SECOND, THIRD AND FORTH LINES INPUT DATA -----
C----- CALL FRICMS ('CLRSQRN ')
      WRITE (6,580)
      READ (5,*)
      IF (ANS .GE. 2) GC TO 40
      WRITE (6,581)
      WRITE (6,582) I (FIT(I),COV(I),P10(I)), I=1,M)
      WRITE (6,590)
      READ (5,*)
      IF (ANS .EQ. 1) GO TO 20
40    CONTINUE

C----- FIFTH LINE INPUT DATA--MACH NO., YAW ANGLE, AOA, SKIN FRICTION DRAG -----
C----- CALL FRICMS ('CLRSQRN ')
      WRITE (6,450)
      WRITE (6,600)
      READ (5,*)
      WRITE (6,610) FMACH
      READ (5,*)
      WRITE (6,620) YA
      READ (5,*)
      WRITE (6,620) AL
      WRITE (6,630)
      READ (5,*)
      CD0

C----- SUMMARY OF FIFTH LINE INPUT DATA -----
C----- CALL FRICMS ('CLRSQRN ')
      WRITE (6,640)
      READ (5,*)
      IF (ANS .GE. 2) GC TO 50
      WRITE (6,641)
      WRITE (6,642) FMACH, YA, AL, CD0

```

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      WRITE (6,650)
      READ (5,*),ANS
      IF (ANS.EQ.1) GO TO 40
      50  CONTINUE
C-----SIXTH LINE INPUT DATA--WING PLANFORM SYMMETRY, NUMBER OF SECTIONS,
C-----SWEEP, DIHEDRAL ANGLE AND FUSELAGE RADIUS
C-----CALL FRICMS (' CLRS CRN ')
      WRITE (6,450)
      WRITE (6,60)
      READ (5,*),ZSYM
      WRITE (6,670)
      READ (5,*),FNS
      WRITE (6,680)
      READ (5,*),SWEEP
      WRITE (6,690)
      READ (5,*),DIHED
      WRITE (6,700)
      READ (5,*),FUS
C-----SUMMARY OF SIXTH LINE INPUT DATA
C-----CALL FRICMS (' CLRS CRN ')
      WRITE (6,710)
      READ (5,*),ANS
      IF (ANS.GE.*2) GO TO 60
      WRITE (6,711)
      WRITE (6,712) ZSYM,FNS,SWEEP,DIHED,FUS
      WRITE (6,720)
      READ (5,*),ANS
      IF (ANS.EQ.1) GO TO 50
      60  CONTINUE
C-----WRITE JCL CARDS TO TOP OF FILE ON USER'S "A" DISK
C-----WRITE (6,120)
      WRITE (6,1210)
C-----WRITE FIRST SIX LINES OF DATA TO FILE ON USER'S "A" DISK
C-----WRITE (6,1010) TITLE
      WRITE (6,1020)
      WRITE (6,1020) FNX,FNY,FNZ,FMESH,FFLCT
      WRITE (6,1040) ((FIT(I),COVOLI),P10(I)),I=1,M)
      WRITE (6,1050)
      WRITE (6,1060)
      WRITE (6,1070) FMACH,YA,AL,CDO

```

-----  
C SECTION INFLT DATA  
C-----

N = IFIX(FNS) \* CLRSCRN \*)  
CALL FR1CHS (\* CLRSCRN \*)  
WRITE (6,45C)  
WRITE (6,730)  
WRITE (6,410)  
DO 200 I=1,N  
WRITE (6,760) 1  
WRITE (6,770)  
READ (5,\*),S  
READ (5,\*),XL  
READ (5,\*),YL  
READ (5,\*),CRD  
READ (5,\*),C1  
READ (5,\*),THICK  
READ (5,\*),AT  
READ (5,\*),FSEC  
CALL FR1CHS (\* CLRSCRN \*)  
WRITE (6,830)  
READ (5,\*),FSEC  
WRITE (6,1100)  
IF (FSEC \* EQ 0.0) GO TO 190  
CALL FR1CHS (\* CLRSCRN \*)  
WRITE (6,450)

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WRLITE (8,1140) ((FPXP(J),FPYP(J)),J=1,FPRNUM)
CCNRITE(190) NUE (8,1120) SYMFN
CCNRITE(190) (8,1130) ((SYMXP(J),SYMP(J)),J=1,SYMMUM)
CCNRITE(190) NUE (8,1140) ((SYMXP(J),SYMP(J)),J=1,SYMMUM)
CCNRITE(190) NUE (8,1150) ((SCWXP(J),SCWP(J)),J=1,SCWNUM)
CCNRITE(190) NUE (8,1120) SCHFN
CCNRITE(190) NUE (8,1130) N572FN
CCNRITE(190) NUE (8,1140) ((N572XP(J),N572YP(J)),J=1,N57NUM)
CCNRITE(190) NUE (8,1150) ((N572XP(J),N572YP(J)),J=1,N57NUM)
CCNRITE(190) NUE (8,1120) F14FN
CCNRITE(190) NUE (8,1130) F14FN
CCNRITE(190) NUE (8,1140) ((F14XP(J),F14YP(J)),J=1,F14NUM)
CCNRITE(190) NUE (8,1150) ((F14XP(J),F14YP(J)),J=1,F14NUM)
CCNRITE(190) NUE (8,1120) A7FN
CCNRITE(190) NUE (8,1130) A7FN
CCNRITE(190) NUE (8,1140) ((A7XP(J),A7YP(J)),J=1,A7NUM)
CCNRITE(190) NUE (8,1150) ((A7XP(J),A7YP(J)),J=1,A7NUM)
CCNRITE(190) NUE (8,1120) LISFN
CCNRITE(190) NUE (8,1130) ((LISXP(J),LISYP(J)),J=1,LISNUM)
CCNRITE(190) NUE (8,1140) ((LISXP(J),LISYP(J)),J=1,LISNUM)
CCNRITE(190) NUE (8,1150) ((LISXP(J),LISYP(J)),J=1,LISNUM)
CCNRITE(190) NUE (8,1120) N1CFN
CCNRITE(190) NUE (8,1130) ((N10XP(J),N10YP(J)),J=1,N10NUM)
CCNRITE(190) NUE (8,1140) ((N10XP(J),N10YP(J)),J=1,N10NUM)
CCNRITE(190) NUE (8,1150) ((N10XP(J),N10YP(J)),J=1,N10NUM)
CCNRITE(190) NUE (8,1120) N34FN
```

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90      WRITE(8,1146) ((N34XP(J),N34YP(J)),J=1,N34NUM)
GCCNTINE(8,1150) N35FN
GCCNTINE(8,1120)
GCCNTINE(8,1130)
GCCNTINE(8,1140)
GCCNTINE(8,1150) ((N35XP(J),N35YP(J)),J=1,N35NUM)

91      CCRITENE(8,1120) N64FN
CCRITENE(8,1130)
CCRITENE(8,1140) ((N64XP(J),N64YP(J)),J=1,N64NUM)
CCRITENE(8,1150) N66FN
CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140)
CCRITENE(8,1150) ((N66XP(J),N66YP(J)),J=1,N66NUM)

92      CCRITENE(8,1120)
CCRITENE(8,1130) N16FN
CCRITENE(8,1140)
CCRITENE(8,1150) ((N16XP(J),N16YP(J)),J=1,N16NUM)
CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140)
CCRITENE(8,1150) ((N16XP(J),N16YP(J)),J=1,N16NUM)

93      CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140) N63FN
CCRITENE(8,1150) ((N63XP(J),N63YP(J)),J=1,N63NUM)
CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140)
CCRITENE(8,1150) ((N63XP(J),N63YP(J)),J=1,N63NUM)

94      CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140) N63AFN
CCRITENE(8,1150) ((N63AXP(J),N63AYP(J)),J=1,N63AN)
CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140)
CCRITENE(8,1150) ((N640XP(J),N640YP(J)),J=1,N64ON)

95      CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140) N640FN
CCRITENE(8,1150) ((N640XP(J),N640YP(J)),J=1,N64ON)
CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140)
CCRITENE(8,1150) ((N640XP(J),N640YP(J)),J=1,N64ON)

96      CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140) N64AFN
CCRITENE(8,1150) ((N640XP(J),N640YP(J)),J=1,N64ON)
CCRITENE(8,1120)
CCRITENE(8,1130)
CCRITENE(8,1140)
CCRITENE(8,1150) ((N640XP(J),N640YP(J)),J=1,N64ON)

97      CCRITENE(8,1120)
CCRITENE(8,1130) N64AFN

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      WRITE (8,1140) ((N64AXP(J),N64AYP(J)),J=1,N64AN)
      WRITE (8,1150) ((N64AXP(J),N64AYP(J)),J=1,N64AN)
      GCNTINE
      KRITE (8,1120) N650FN
      KRITE (8,1130) N650FN
      KRITE (8,1140) ((N650XP(J),N650YP(J)),J=1,N650N)
      KRITE (8,1150) ((N650XP(J),N650YP(J)),J=1,N650N)
      GCNTINE
      KRITE (8,1120) N65AFN
      KRITE (8,1130) N65AFN
      KRITE (8,1140) ((N65AXP(J),N65AYP(J)),J=1,N65AN)
      GCNTINE
      KRITE (8,1120) N660FN
      KRITE (8,1130) N660FN
      KRITE (8,1140) ((N660XP(J),N660YP(J)),J=1,N660N)
      KRITE (8,1150) ((N660XP(J),N660YP(J)),J=1,N660N)
      GCNTINE
      CALL FR7CMS ('CLRSCRN ')
      100   CONTINUE
      C-- WRITE THREE LINES TO USER'S FILE INDICATING END OF CALCUL
      C-- WRITE ((E,1160)
      C-- WRITE ((E,1170)
      C-- WRITE ((E,1180) ZERC
      C-- WRITE JCL CARDS TO BOTTOM OF FILE IN USER'S "A" DISK
      C-- WRITE ((E,1220)
      C-- WRITE ((E,1230)
      C-- INDICATE TO USER THAT INPUT IS COMPLETE
      C-- CALL FR7CMS ('CLRSCRN ')
      C-- FORMAT STATEMENTS
      C-- RETURN
      110   FORMAT (1X,79H

```



580 FORMAT (1X,5SH SUMMARY CF SECTION, THIRD AND FORTH LINES OF INPUT DATA  
 1 ITA2.1/1X125H=) ENTER 1 = YES; 2 = NO  
 581 FORMAT (1X,3HF IT17X14HCVO,6X,3HF10)  
 582 FORMAT (1X,F5.15XF7.6,3XF3.1) THIRD AND FORTH LINES INPUT DATA?  
 590 1 /1X\*25H=) ENTER 1 = YES; 2 = NO  
 1 FORMAT (1X,46H=) ENTER FREE STREAM MACH NUMBER (FMACH) : (R)  
 600 1 FORMAT (1X,40H=) ENTER YAW ANGLE IN DEGREES (YAW) : (R)  
 610 1 FORMAT (1X,46H=) ENTER ATTACK IN DEGREES (AL) : (R)  
 620 1 FORMAT (1X,58H=) ENTER DRAG COEFFICIENT DUE TO FRICTION (CD0)  
 630 1 : (R) , (15X,48H) (UNLESS OTHERWISE AVAILABLE C01 IS RECOMMENDED)  
 1 FORMAT (1X,33H SUMMARY OF FIFTH LINE INPUT DATA?,/1X,25H=) ENTER  
 640 1 YES; 2 = NO  
 1 FORMAT (1X,5HF MACH .5X,2HYA,8X,2HAL,8X,3FCDO)  
 641 FORMAT (1X,52H=) ENTER WING PLANFORM SYMMETRY TRIGGER (ZSYM) : (R)  
 642 FORMAT (1X,29H CHANGE FIFTH LINE INPUT DATA?,/1X,25H=) ENTER 1 =  
 650 1 YES; 2 = NO  
 660 1 FORMAT (1X,52H=) ENTER WING HAS SPANWISE SYMMETRY ./,1X,38H1.0 = S  
 1 /1X,41H0.0 = SPANNED WING HAS SPANWISE SYMMETRY  
 2 FORMAT (1X,78H=) ENTER NUMBER OF SECTIONS WHERE WING SECTION GEOM  
 670 1 ENTRY IS DEFINED (FNS) : (R) ./,5X,53F (VALUE MUST BE > QR = 3.0, BUT  
 2 NOT GREATER THAN 1.0) ! ENTER LEADING EDGE SWEET ANGLE IN DEGREES (SWEET  
 1 FORMAT (1X,58H=) ENTER DIHEDRAL ANGLE IN DEGREES (DIHED) : (R)  
 680 1 FORMAT (1X,48H=) ENTER DIHEDRAL ANGLE IN DEGREES (DIHED) : (R)  
 690 1 FORMAT (1X,36H=) ENTER FUSELAGE RADIUS (FUS) : (R) ./,5X,33HNOTE: U  
 700 1 FORMATE (1X,33H SUMMARY OF SIXTH LINE INPUT DATA?,/1X,25H=) ENTER  
 710 1 YES; 2 = NO  
 711 1 FORMAT (1X,4HZ SYM,6X,3HFNS,7X,5HSWEET,5X,5HED,5X,3HFUS)  
 712 FORMAT (1X,17XF4,16X,F6\*3,4XF6,24X,F10\*6,24X,F10\*6,24X,F10\*6,  
 720 1 YES; 2 = NO  
 730 1 FORMAT (1X,66H THE NEXT SET OF INPUT DATA WILL BE REPEATED FOR EACH  
 1 WING SECTION ./,5X,63H AND Y COORDINATES DEFINING THE WING SECTION  
 2 ON SHAPE ARE ENTERED ./,5X,67H STARTING WITH THE UPPER SURFACE TRAIL  
 3ING EDGE AND PROGRESSING AROUND THE 35HTC THE LOWER SURFACE TRAIL  
 4ING EDGE ./,5X,57H AND Y COORDINATES ARE NORMALIZED WITH THE CHORD  
 5 LENGTH ./,5X,46H WING SECTION DEFINING COORDINATES CAN BE INPUT,/br/>
 6 5X,36H THEY THE USER OR SELECTED FROM A MENU.)  
 740 1 FORMAT (28X,23H\*# WING SECTION MENU\*\*\*,/6X,34H0 = USER INPUT SECTION  
 1 LINE COORD DATA ./,6X,19H1 = FLAT PLATE DATA ./,6X,49H2 = SYMMETRIC  
 2 WING THICKNESS AT 30% CHORD ./,6X,61H3 = SUPERCRITICAL WING  
 3 (CAMBERED 11% THICKNESS AT 12% CHORD ./,6X,61H4 = NACA 24-30 (CA  
 4 MBERED 12% THICKNESS AT 30% CHORD ./,6X,52H5 = F14 WING (CAMBERED  
 59.5% THICKNESS AT 37% CHORD ./,6X,66H = A-7 WING (7 DEG DROOP AT  
 620% CHORD, 7% THICKNESS AT 43% CHORD, ./,6X,64H7 = LISSAMAN 7769 A1



2K. IF YOU WISH TO MAKE FURTHER !'5X,62H CHANGES TO YOUR INPUT DATA  
 3SI AND THE CREATED DATA FILE, //5X,61H TO RUN THE POTENTIAL  
 4FLICK PECGRATE ( FLO27 ) USING YOUR DATA FILE //5X,61H XED ITS CUTLINE  
 5AND ENTER ADDITIONAL CARDS (JOBCARD ETC) //5X,60HAS CUTLINE  
 6INSTRUCTIONS. THEN SUBMIT THE FILE TO THE //5X,16HBATCH PR  
 7OCCESSOR. //1X4HBYE.

```

1000 FORMAT(1X16(A4))
1010 FORMAT(3HFNX7X3HFNY7X!3HFNZ7X!3HFNZ,7X!5HFNESH,5X,F3.1)
1020 FORMAT(F5.17X!4HCOVC6X!3HP10)
1030 FORMAT(F5.17X!4HCOVC6X!3HP10)
1040 FORMAT(F5.17X!4HCOVC6X!3HP10)
1050 FORMAT(F5.17X!4HCOVC6X!3HP10)
1060 FORMAT(F5.17X!4HCOVC6X!3HP10)
1070 FORMAT(F5.17X!4HCOVC6X!3HP10)
1080 FORMAT(F4.2SYM6X!3HFNS7X!5HSWEEP5X!5HDIHED5X,3HFUS)
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